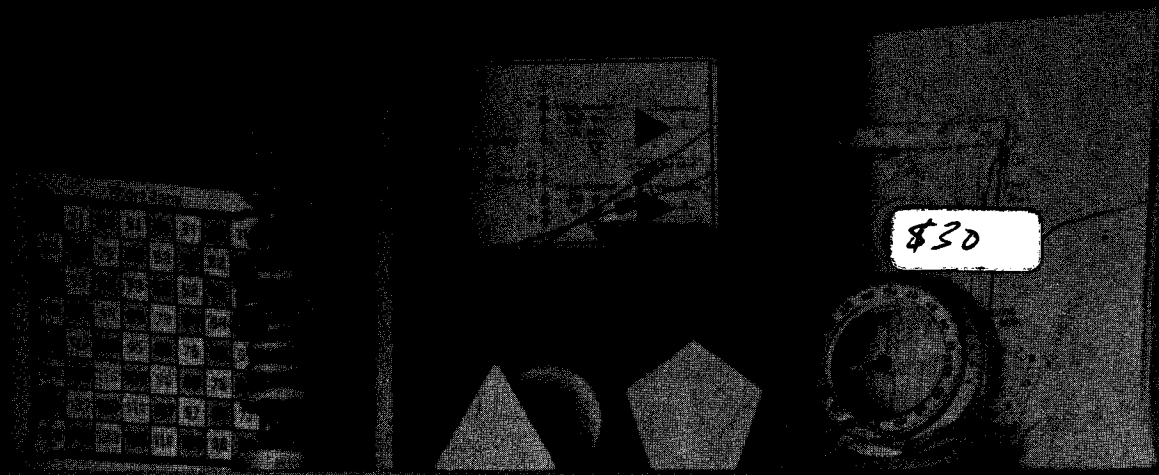
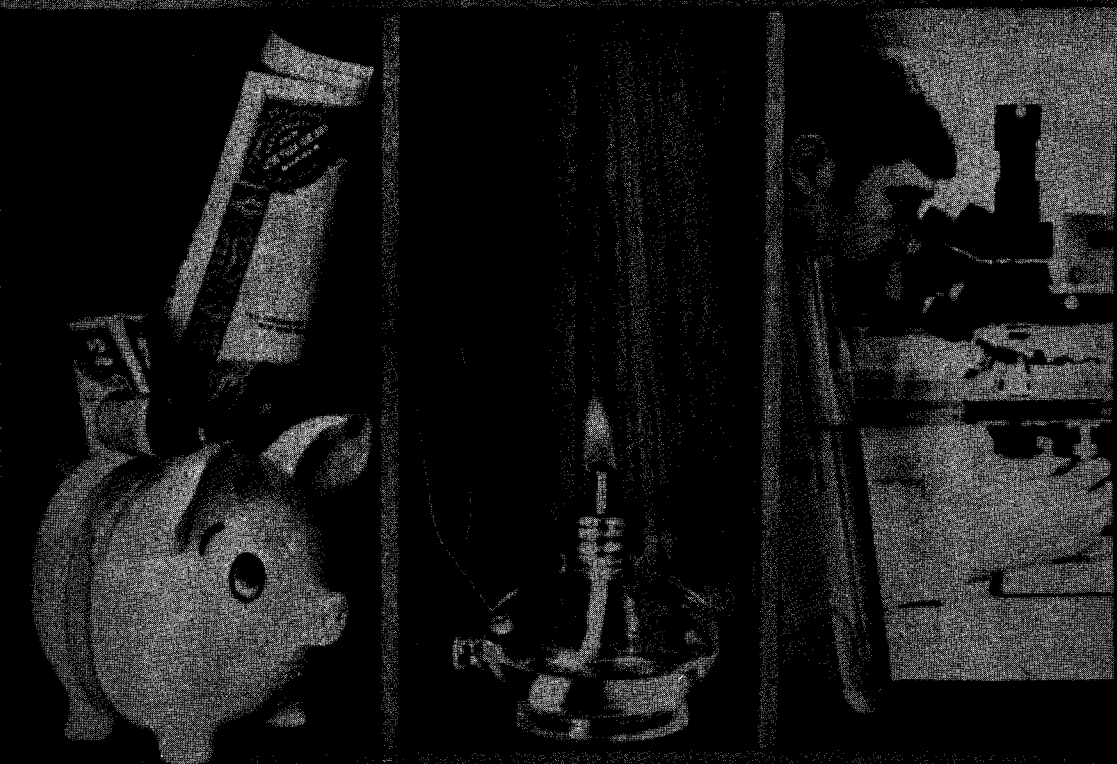




Hewlett-Packard
**HP-19C/HP-29C
SOLUTIONS**

ELECTRICAL ENGINEERING



INTRODUCTION

This HP-19C/HP-29C Solutions book was written to help you get the most from your calculator. The programs were chosen to provide useful calculations for many of the common problems encountered.

They will provide you with immediate capabilities in your everyday calculations and you will find them useful as guides to programming techniques for writing your own customized software. The comments on each program listing describe the approach used to reach the solution and help you follow the programmer's logic as you become an expert on your HP calculator.

You will find general information on how to key in and run programs under "A Word about Program Usage" in the Applications book you received with your calculator.

We hope that this Solutions book will be a valuable tool in your work and would appreciate your comments about it.

The program material contained herein is supplied without representation or warranty of any kind. Hewlett-Packard Company therefore assumes no responsibility and shall have no liability, consequential or otherwise, of any kind arising from the use of this program material or any part thereof.

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RESISTIVE/REACTIVE CIRCUIT CALCULATIONS

This program performs resonance calculations for R-L-C circuits, calculates the reactance of inductive and capacitive branches, the equivalent value of series capacitors or parallel resistors and inductors, and performs power calculations for resistive branches using straightforward manipulations of the following equations:

$$f_r = \frac{1}{2\pi\sqrt{LC}}$$

$$X_C = \frac{1}{2\pi fC}$$

$$X_L = 2\pi fL$$

$$P = I^2R = E^2/R$$

$$\frac{A_1 A_2}{A_1 + A_2} = A_3$$

where

f_r = resonant frequency in hertz

L = inductance in henrys

C = capacitance in farads

X_C = capacitive reactance in Ω

X_L = inductive reactance in Ω

P = power in watts

I = current in amps

R = resistance in Ω

E = voltage in volts

A_1, A_2 = the values of two parallel resistors in ohms, two parallel inductors in henrys, or two series capacitors in farads

A_3 = the resultant, equivalent resistance in ohms, inductance in henrys, or capacitance in farads

NOTE: Given a resistance or capacitance, A_1 , the value of the circuit element required to produce a desired resultant resistance or capacitance may be calculated by entering A_1 as a negative value.

EXAMPLES:

1. $C = .01\mu F$, $L = 160\mu H$.
Calculate f_r
2. $L = 2.5H$, $f_r = 60Hz$
Calculate C and X_L at f_r
3. $E = 345V$, $R = 1.25M\Omega$
Calculate P and I
4. $R_1 = 120\Omega$, $R_2 = 240\Omega$
 - a. Find the equivalent resistance of these two resistors in parallel, R_3 .
 - b. Parallel R_3 with 50Ω .
 - c. Find the resistance required for a resultant resistance of 25Ω .

SOLUTION:

160.-06 ENT1
 0.01-06 GSB1
 125.02+03 *** f_r

60.0000 ENT1
 2.5000 GSB2
 2.8145-06 *** C

60.0000 ENT1
 2.5000 GSB4
 942.46+00 *** X_L

345.0000 ENT1
 1.25+06 GSB5
 95.220-03 *** P

1.25+06 GSB7
 276.00-06 *** I

120.0000 ENT1
 240.0000 GSB9
 80.000+00 *** R_3

50.0000 GSB3
 30.769+00 *** 4b

CH5
 25.0000 GSB3
 133.33+00 *** 4c

Program Listings

01 *LBL1					
02 X					
03 JX					
04 GT00					
05 *LBL2					
06 X*Y					
07 GSB0					
08 X²					
09 X*Y					
10 ÷					
11 R/S	L or C				
12 *LBL3					
13 X					
14 GT00					
15 *LBL4					
16 X					
17 GSB0					
18 1/X					
19 R/S	X _L				
20 *LBL5					
21 1/X					
22 *LBL6					
23 X*Y					
24 X²					
25 X					
26 R/S	P				
27 *LBL7					
28 1/X					
29 *LBL8					
30 X					
31 JX					
32 R/S	I or E				
33 *LBL9					
34 2					
35 X					
36 Pi					
37 X					
38 1/X					
39 RTN	f _r or X _C				
40 *LBL9					
41 X					
42 ENT↑					
43 ENT↑					
44 LSTX					
45 ÷					
46 LSTX					
47 +					
48 ÷					
49 R/S	A ₃ or A ₂				
*** "Printx" may be inserted or used to replace "R/S".					
REGISTERS					
0	1	2	3	4	5
6	7	8	9	.0	.1
.2	.3	.4	.5	16	17
18	19	20	21	22	23
24	25	26	27	28	29

IMPEDANCE OF A LADDER NETWORK

This program computes the input impedance of an arbitrary ladder network. Elements are added one at a time starting from the right. The first element must be in parallel.

Suppose we have a network whose input admittance is Y_{in} . Adding a shunt R, L, or C, the input admittance becomes

$$Y_{new} = \begin{cases} Y_{in} + \left(\frac{1}{R} + j0\right) \\ Y_{in} + \left(0 - j \frac{1}{\omega L_p}\right) \\ Y_{in} + (0 + j \omega C_p) \end{cases}$$

Adding a series R, L, or C, we have

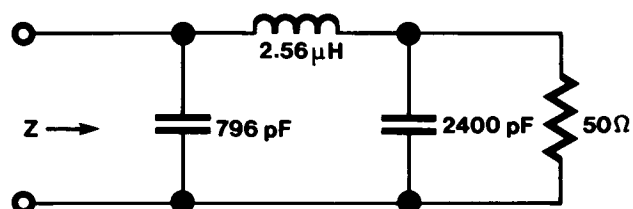
$$Y_{new} = \begin{cases} \left(\frac{1}{Y_{in}} + (R_s + j0)\right)^{-1} \\ \left(\frac{1}{Y_{in}} + (0 + j \omega L_s)\right)^{-1} \\ \left(\frac{1}{Y_{in}} + \left(0 - j \frac{1}{\omega C_s}\right)\right)^{-1} \end{cases}$$

The program converts this admittance to an impedance for display.

NOTE: An erroneous entry may be corrected by entering the negative of the incorrect value.

EXAMPLE:

$$f = 4 \text{ MHz}$$



SOLUTION:

```

      FIX2
4.+06 GSB1
50.00 GSB3 |Zin|
50.00 ***
X=Y
0.00 *** ∠Zin
2400.-12 GSB5
15.74 *** |Zin|
X=Y
-71.66 *** ∠Zin
2.56-06 GSB2
GSB5
49.65 *** |Zin|
X=Y
84.28 *** ∠Zin
796.-12 GSB5
497.69 *** |Zin|
X=Y
0.98 *** ∠Zin

```


Program Listings

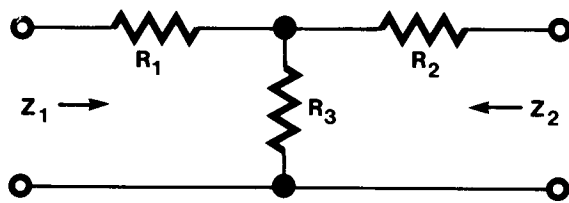
7

01 *LBL1	f	50 GSB0	Convert $Y_{in} \rightarrow Z_{in}$
02 2		51 R↓	
03 x		52 RCL6	
04 Pi		53 +	} Add admittances or impedances
05 x	Clear flag	54 X≠Y	
06 CLRG	w	55 RCL7	
07 ST03		56 +	
08 R/S		57 X≠Y	
09 *LBL0	$Z \leftrightarrow Y$	58 RCL0	
10 R↓		59 X≠0?	
11 +P		60 GSB0	
12 1/X		61 R↓	Convert Z→Y
13 X≠Y		62 ST01	
14 CHS		63 X≠Y	
15 X≠Y		64 ST02	
16 +R		65 X≠Y	
17 0		66 0	
18 RTN	R,C,L	67 GSB0	Convert Y→Z
19 *LBL2	Set flag (series)	68 ST00	Clear flag
20 ST00		69 R↓	
21 R/S		70 +P	
22 *LBL3		71 R/S	
23 1/X			*** $ Z_{in} \angle Z_{in}$
24 RCL0			
25 X≠0?	0,Y (parallel)		
26 GT08			
27 0			
28 GT08			
29 *LBL4	0,Z (series)		
30 RCL3			
31 x			
32 1/X	X_C or B_L		
33 CHS			
34 0			
35 X≠Y			
36 GT08			
37 *LBL5			
38 RCL3			
39 x	X_L or B_C		
40 0			
41 X≠Y			
42 *LBL8			
43 ST07			
44 X≠Y			
45 ST06			
46 RCL2			
47 RCL1			
48 RCL0			
49 X≠0?			
		*** "Printx" may be inserted.	

REGISTERS					
0 flag	1 Re[Y_{in}]	2 Im[Y_{in}]	3 $\omega = 2\pi f$	4	5
6 used	7 used	8	9	10	11
12	13	14	15	16	17
18	19	20	21	22	23
24	25	26	27	28	29

T ATTENUATOR

The T attenuator can be used to match between two impedances, Z_1 and Z_2 . This program computes the minimum loss of the attenuator and values for the resistors R_1 , R_2 , and R_3 which will yield an attenuator having any desired loss.



The minimum loss in decibels is given by

$$\text{Min Loss} = 10 \log \left(\sqrt{\frac{Z_1}{Z_2}} + \sqrt{\frac{Z_1}{Z_2} - 1} \right)^2$$

where

$$Z_1 \geq Z_2$$

If N is the desired loss of the attenuator expressed as a ratio (loss in dB = $10 \log N$), then

$$R_3 = \frac{2\sqrt{NZ_1Z_2}}{N-1}$$

$$R_1 = Z_1 \left(\frac{N+1}{N-1} \right) - R_3$$

$$R_2 = Z_2 \left(\frac{N+1}{N-1} \right) - R_3$$

NOTE: If the desired loss is less than the minimum loss R_2 will be negative.

EXAMPLE:

$$Z_1 = 75\Omega$$

$$Z_2 = 50\Omega$$

$$\text{Loss} = 6 \text{ dB}$$

SOLUTION:

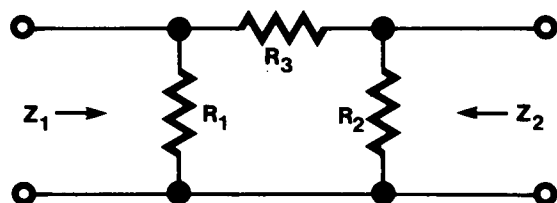
75.0000	ENT1	
50.0000	GSE1	
6.0000	GSE2	
5.7195+00	***	Min Loss
	R/S	
43.344+00	***	R ₁
	R/S	
1.5715+00	***	R ₂
	R/S	
81.973+00	***	R ₃

Program Listings

01 *LBL1 02 ENG4 03 ST02 04 X*Y 05 ST01 06 R/S 07 *LBL2 08 1 09 0 10 ÷ 11 10* 12 ST07 13 X 14 X 15 JX 16 2 17 X 18 RCL7 19 1 20 ST+7 21 - 22 ST08 23 ÷ 24 ST05 25 RCL1 26 RCL7 27 X 28 RCL8 29 ÷ 30 RCL5 31 - 32 ST03 33 RCL2 34 RCL7 35 X 36 RCL8 37 ÷ 38 RCL5 39 - 40 ST04 41 RCL1 42 RCL2 43 ÷ 44 ENT↑ 45 JX 46 X*Y 47 1 48 - 49 JX	N
--	---

PI ATTENUATOR

The PI attenuator can be used to match between two impedances, Z_1 and Z_2 . This program computes the minimum loss of the attenuator and values for the resistors R_1 , R_2 , and R_3 which will yield an attenuator having any desired loss.



The minimum loss in decibels is given by

$$\text{Min Loss} = 10 \log \left(\sqrt{\frac{Z_1}{Z_2}} + \sqrt{\frac{Z_1}{Z_2} - 1} \right)^2$$

where $Z_1 \geq Z_2$

If N is the desired loss of the attenuator expressed as a ratio (loss in $\text{dB} = 10 \log N$), then

$$R_3 = \frac{1}{2}(N-1) \left(\frac{Z_1 Z_2}{N} \right)^{1/2}$$

$$\frac{1}{R_1} = \frac{1}{Z_1} \left(\frac{N+1}{N-1} \right) - \frac{1}{R_3}$$

$$\frac{1}{R_2} = \frac{1}{Z_2} \left(\frac{N+1}{N-1} \right) - \frac{1}{R_3}$$

EXAMPLE:

$$Z_1 = 75\Omega$$

$$Z_2 = 50\Omega$$

$$\text{Loss} = 6\text{dB}$$

SOLUTION:

```

75.0000 EN71
50.0000 GS81
6.0000 GS22
5.7195+00 *** Min Loss
                R/S
2.3862+03 *** R1
                R/S
86.517+00 *** R2
                R/S
45.747+00 *** R3

```


Program Listings

13

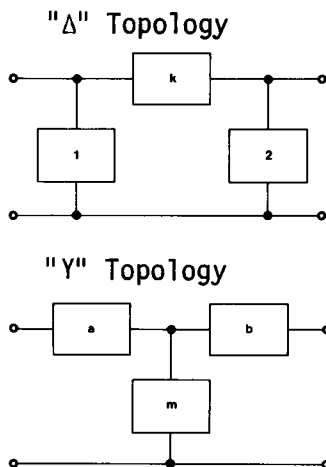
01 *LBL1		50 X2	
02 ENG4		51 LOG	
03 ST02		52 1	
04 X2Y		53 0	
05 ST01		54 X	
06 R/S		55 ST06	
07 *LBL2		56 R/S	*** Min Loss
08 1		57 RCL3	
09 0		58 R/S	*** R ₁
10 ÷		59 RCL4	*** R ₂
11 10*		60 R/S	*** R ₃
12 ST07	N	61 RCL5	
13 ÷		62 R/S	
14 X			
15 JX			
16 RCL7			
17 1			
18 ST+7			
19 -			
20 ST÷7			
21 2			
22 ÷			
23 X			
24 ST05	R ₃		
25 1/X			
26 ST08			
27 RCL7			
28 RCL1			
29 ÷			
30 RCL8			
31 -			
32 1/X			
33 ST03	R ₁		
34 RCL7			
35 RCL2			
36 ÷			
37 RCL8			
38 -			
39 1/X			
40 ST04	R ₂		
41 RCL1			
42 RCL2			
43 ÷			
44 JX			
45 LSTX			
46 1			
47 -			
48 JX			
49 +			

REGISTERS					
0	1 Z ₁	2 Z ₂	3 R ₁	4 R ₂	5 R ₃
6 Min Loss	7 $N, \frac{N+1}{N-1}$	8 1/R ₃	9	10	11
12	13	14	15	16	17
18	19	20	21	22	23
24	25	26	27	28	29

WYE-DELTA OR DELTA-WYE TRANSFORMATION

This program performs the Y- Δ transform for circuits consisting of resistors, inductors, or capacitors*.

The Y- Δ transforms for one-of-a-kind elements are summarized below.



For Capacitors:

$$Y \rightarrow \Delta \quad C_1 = \frac{C_a C_m}{\Sigma C}$$

$$C_2 = \frac{C_b C_m}{\Sigma C}$$

$$C_k = \frac{C_a C_b}{\Sigma C}$$

$$\Sigma C = C_a + C_b + C_m$$

$$\Delta \rightarrow Y \quad C_a = \frac{\Sigma CC}{C_2}$$

$$C_b = \frac{\Sigma CC}{C_1}$$

$$C_m = \frac{\Sigma CC}{C_k}$$

$$\Sigma CC = C_1 C_2 + C_2 C_k + C_1 C_k$$

For Inductors: (and Resistors, replace L's by R's)

$$Y \rightarrow \Delta \quad L_1 = \frac{\Sigma LL}{L_b}$$

$$L_2 = \frac{\Sigma LL}{L_a}$$

$$L_k = \frac{\Sigma LL}{L_m}$$

$$\Sigma LL = L_a L_b + L_b L_m + L_a L_m$$

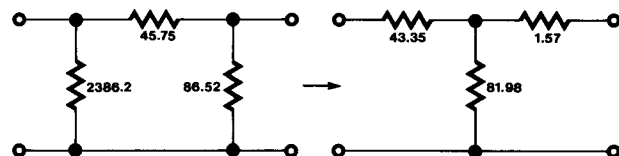
$$\Delta \rightarrow Y \quad L_a = \frac{L_1 L_k}{\Sigma L}$$

$$L_b = \frac{L_2 L_k}{\Sigma L}$$

$$L_m = \frac{L_1 L_2}{\Sigma L}$$

$$\Sigma L = L_1 + L_2 + L_k$$

EXAMPLE:



SOLUTION:

2386.20	ENT↑	1
45.75	ENT↑	k
86.52	G5B1	2
	G5B2	
	G5B4	a
43.35	***	
	R/S	m
81.98	***	
	R/S	b
1.57	***	

* Adapted from HP-67/97 Users' Library program #00404D by Bruce Murdock.

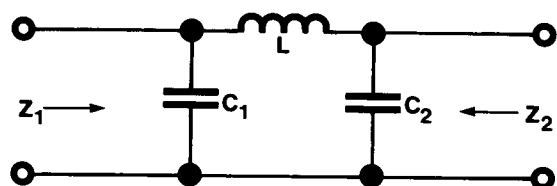
Program Listings

01 *LBL1		50 RCL2	
02 ST03		51 X	
03 R1		52 RCL2	
04 ST02		53 RCL3	
05 R4		54 X	
06 ST01		55 +	
07 0	Clear flag to indicate capacitors	56 RCL1	
08 ST00		57 RCL3	
09 R/S		58 X	
10 *LBL2		59 +	
11 1	Set flag to indi- cate inductors or resistors	60 ST04	$\Sigma\Sigma$
12 ST00	Y $\rightarrow$ Δ for capacitors or $\Delta\rightarrow$ Y for resistors and inductors	61 RCL3	
13 R/S		62 ÷	
14 *LBL3		63 ST05	
15 RCL0		64 RCL4	
16 X>0?		65 RCL2	
17 GT00		66 ÷	
18 *LBL9		67 ST06	
19 RCL1		68 RCL4	
20 RCL2		69 RCL1	
21 +		70 ÷	
22 RCL3		71 ST07	
23 +	Σ	72 *LBL8	Output
24 ST04		73 RCL5	*** 1 or a
25 RCL1		74 R/S	
26 RCL2		75 RCL6	
27 X		76 R/S	*** k or m
28 RCL4		77 RCL7	
29 ÷		78 R/S	*** 2 or b
30 ST05			
31 RCL1			
32 RCL3			
33 X			
34 RCL4			
35 ÷			
36 ST06			
37 RCL2			
38 RCL3			
39 X			
40 RCL4			
41 ÷			
42 ST07			
43 GT08			
44 *LBL4	$\Delta\rightarrow$ Y for capacitors or Y $\rightarrow$ Δ for resistors and inductors	*** "Printx" may replace "R/S".	
45 RCL0			
46 X>0?			
47 GT09			
48 *LBL0			
49 RCL1			

REGISTERS					
0 flag	1 1 or a	2 k or m	3 2 or b	4 Σ or $\Sigma\Sigma$	5 1 or a
6 k or m	7 2 or b	8	9	.0	.1
.2	.3	.4	.5	16	17
18	19	20	21	22	23
24	25	26	27	28	29

PI NETWORK IMPEDANCE MATCHING

A lossless network is often used to match between two resistive impedances Z_1 and Z_2 , as shown



Given the values of Z_1 and Z_2 ($Z_1 > Z_2$) the frequency f , and the desired circuit Q , the values of C_1 , C_2 , and L can be found from the following formulas:

$$X_{C1} = \frac{Z_1}{Q} \qquad C_1 = \frac{1}{2\pi f X_{C1}}$$

$$X_{C2} = \frac{Z_2}{\left[\frac{Z_2}{Z_1} (Q^2 + 1) - 1 \right]^{1/2}} \qquad C_2 = \frac{1}{2\pi f X_{C2}}$$

$$X_L = \frac{Q Z_1}{Q^2 + 1} \left[1 + \frac{Z_2}{Q X_{C2}} \right] \qquad L = \frac{X_L}{2\pi f}$$

NOTE: Z_1 , Z_2 , and Q must be chosen so that

$$\frac{Z_2}{Z_1} (Q^2 + 1) > 1$$

EXAMPLE:

$$Z_1 = 500\Omega$$

$$Z_2 = 50\Omega$$

$$f = 4\text{MHz}$$

$$Q = 10$$

SOLUTION:

```

500.0000 ENT↑
50.0000 ENT↑
4.+06 ENT↑
10.0000 GSB1
795.77-12 *** C1
R/S
2.4006-09 *** C2
R/S
2.5639-06 *** L
  
```


Program Listings

19

01 *LBL1		50 R/S	***C ₁ ,C ₂ ,L
02 ST04		51 RTN	
03 R4		52 R/S	
04 ST03			
05 R4			
06 ST02			
07 R4			
08 ST01			
09 ENG4			
10 RCL4			
11 RCL1			
12 ÷			
13 GSB0			
14 RCL2			
15 RCL1			
16 ÷			
17 RCL4			
18 X²			
19 1			
20 +			
21 ST05			
22 x			
23 1			
24 -			
25 JX			
26 RCL2	1/X _{C₂}		
27 ÷			
28 ST06			
29 GSB0			
30 RCL2			
31 RCL6			
32 x			
33 RCL4			
34 ÷			
35 1			
36 +			
37 RCL4			
38 RCL1			
39 x			
40 RCL5			
41 ÷			
42 x			
43 *LBL0			
44 Pi			
45 2			
46 x			
47 RCL3			
48 x			
49 ÷			

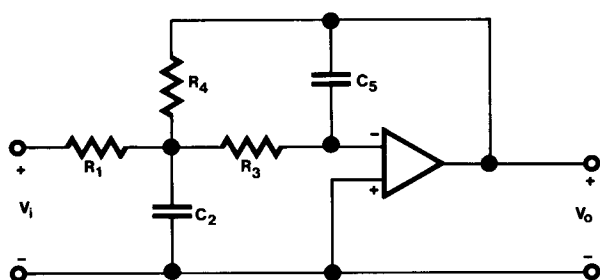
REGISTERS

0	1 Z ₁	2 Z ₂	3 f	4 Q	5 Q ² +1
6 1/X _{C₂}	7	8	9	.0	.1
.2	.3	.4	.5	16	17
18	19	20	21	22	23
24	25	26	27	28	29

ACTIVE FILTER DESIGN

The transfer function of the active low-pass filter shown is

$$\frac{V_o}{V_i}(s) = \frac{-\frac{1}{R_1 R_3 C_2 C_5}}{s^2 + \frac{s}{C_2} \left(\frac{1}{R_1} + \frac{1}{R_3} + \frac{1}{R_4} \right) + \frac{1}{R_3 R_4 C_2 C_5}}$$



Given

$$G = \left| \frac{V_o}{V_i} \right|, \text{ the desired low frequency gain}$$

f_c , the cutoff frequency in hertz

α , the desired "alpha peaking factor" ($\alpha = 2\zeta$, where ζ is the damping factor)

$C = C_5$, farads

the program computes values for R_1 , C_2 , R_3 and R_4 according to the following equations:

$$R_4 = \frac{\alpha}{4\pi f_c C}$$

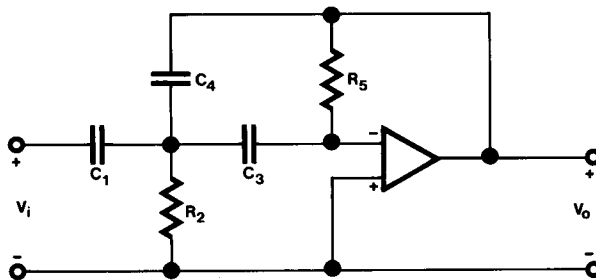
$$R_1 = \frac{R_4}{G}$$

$$R_3 = \frac{R_4}{G + 1}$$

$$C_2 = \frac{G + 1}{R_4 \alpha \pi f_c}$$

The transfer function of the active high-pass filter shown is

$$\frac{V_o}{V_i}(s) = \frac{-s^2 \frac{C_1}{C_4}}{s^2 + \frac{s}{R_5} \left(\frac{C_1}{C_3 C_4} + \frac{1}{C_4} + \frac{1}{C_3} \right) + \frac{1}{R_2 R_5 C_3 C_4}}$$



Given

$$G = \left| \frac{V_o}{V_i} \right|, \text{ the desired high frequency gain}$$

f_c

α

$C = C_1 = C_3$, farads

this program solves the following equations for the values of R_2 , R_5 , and C_4 .²

$$R_2 = \frac{\alpha}{2\pi f_c C \left(2 + \frac{1}{G} \right)}$$

$$R_5 = \frac{2G + 1}{\alpha 2\pi f_c C}$$

$$C_4 = \frac{C}{G}$$

NOTES: 1. If α is not specified, $\alpha = \sqrt{2}$ is used, giving component values for a Butterworth filter.

2. These equations derive from the fact that both transfer functions have the form

$$H(s) = \frac{-G \omega_c^2}{s^2 + 2\omega_c s + \omega_c^2},$$

EXAMPLES:

1. Compute R_4 , R_1 , R_3 , and C_2 for a low-pass filter with

$$f_c = 100 \text{ Hz}$$

$$C = .1 \mu\text{F}$$

$$G = 10$$

$$\alpha = \sqrt{2}$$

2. Compute R_2 , C_4 , and R_5 for a high-pass filter with

$$f_c = .1 \text{ Hz}$$

$$C = 10 \mu\text{F}$$

$$G = 1$$

$$\alpha = \sqrt{2}$$

SOLUTIONS:

```

FIX2
100.00 ENT↑
0.1-06 ENT↑
10.00 ENT↑
2.00 JX
GSB1
11253.95 *** R4
R/S
1125.40 *** R1
R/S
1023.09 *** R3
R/S
2.20-06 *** C2

```

```

0.10 ENT↑
10.-06 ENT↑
1.00 ENT↑
2.00 JX
GSB2
75026.36 *** R2
R/S
1.00-05 *** C4
R/S
337618.62 *** R5

```


User Instructions

[illegible]

Program Listings

23

01 *LBL1		50 ÷	
02 ST07		51 R/S	*** R ₂
03 R↓		52 RCL6	
04 R↓		53 RCL5	
05 ST06		54 ST÷7	
06 x		55 ÷	
07 Pi		56 R/S	*** C ₄
08 x		57 RCL7	
09 4		58 1/X	
10 x		59 R/S	*** R ₅
11 ÷			
12 R/S			
13 ST04	*** R ₄		
14 X÷Y			
15 ÷			
16 R/S	*** R ₁		
17 RCL4			
18 LSTX			
19 1			
20 +			
21 ÷			
22 R/S	*** R ₃		
23 LSTX			
24 RCL6			
25 x			
26 4			
27 x			
28 RCL7			
29 X²			
30 ÷			
31 R/S	*** C ₂		
32 *LBL2			
33 ST07			
34 R↓			
35 ST05			
36 R↓			
37 ST06			
38 x			
39 2			
40 x			
41 Pi			
42 x			
43 STx7			
44 RCL5			
45 1/X			
46 2	(2 G+1)/G		
47 +			
48 ST÷7			
49 x			

REGISTERS

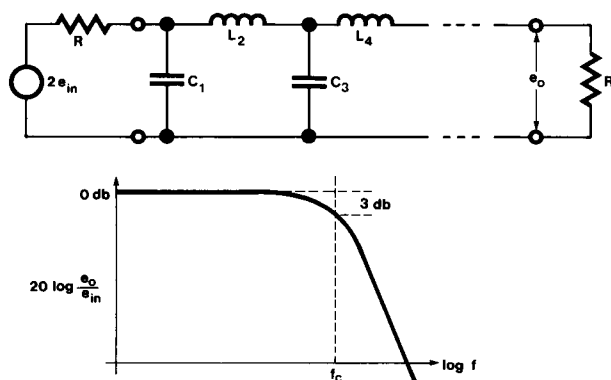
0	1	2	3	4 R ₄	5 G
6 C	7 α	8 2 G+1	9	.0	.1
.2	.3	.4	.5	16	17
18	19	20	21	22	23
24	25	26	27	28	29

BUTTERWORTH FILTER DESIGN

This program computes component values for Butterworth low-pass filters between equal terminations given filter order, termination resistance in ohms, and corner frequency in hertz.

$$C_i = \frac{1}{\pi f_c R} \sin \frac{(2i-1)\pi}{2n}, \quad i = 1, 3, 5, \dots$$

$$L_i = \frac{R}{\pi f_c} \sin \frac{(2i-1)\pi}{2n}, \quad i = 2, 4, 6, \dots$$



NOTE: $n \leq 10$

EXAMPLE:

$$n = 6$$

$$R = 50\Omega$$

$$f_c = 10 \text{ MHz}$$

SOLUTION:

```

6.0000 ENT↑
50.0000 ENT↑
10.+06 GSE1
1.0000+00 *** i
R/S
164.77-12 *** C1
R/S
2.0000+00 ***
R/S
1.1254-06 *** L2
R/S
3.0000+00 ***
R/S
614.93-12 *** C3
R/S
4.0000+00 ***
R/S
1.5373-06 *** L4
R/S
5.0000+00 ***
R/S
450.16-12 *** C5
R/S
6.0000+00 ***
R/S
411.92-09 *** L6

```

User Instructions

[illegible]

Program Listings

01 *LBL1 02 RAD 03 ENG4 04 ST.3 05 R↓ 06 ST.2 07 R↓ 08 ST.1 09 ST00 10 *LBL0 11 RCL0 12 2 13 x 14 1 15 - 16 Pi 17 x 18 RC.1 19 2 20 x 21 ÷ 22 ST0i 23 DSZ 24 GT00 25 Pi 26 RC.3 27 RC.2 28 x 29 x 30 1/X 31 ST.5 32 2 33 CHS 34 ST.4 35 1 36 ST00 37 *LBL9 38 RC.1 39 RCL0 40 X>Y? 41 GT08 42 R/S 43 RCLi 44 SIN 45 RC.5 46 x 47 R/S 48 RC.2 49 RC.4	Sine argument
--	---

STANDARD RESISTANCE VALUES*

For a given tolerance, a "step size" is computed which is used to determine two values, one below and one above the non-standard resistance. These are converted by a subroutine to standard values, and the geometric mean of the latter is calculated. If the given non-standard value is below the mean then the lower standard value is selected; otherwise the larger value is selected.

NOTE: Incorrect results will be obtained for tolerances other than 5%, 10%, or 20%.

REFERENCE: International Telephone and Telegraph Corp.
Reference Data for Radio Engineers, fourth edition, p. 78.

EXAMPLES: Find the closest standard values for the following:

$$R_1 = 432\Omega$$

$$R_2 = 114\text{ K}\Omega$$

$$R_3 = 3.5\text{ M}\Omega$$

SOLUTION:

5.0000 GSE1	5%
432.0000 GSE2	
430.00+02 ***	R ₁
114.+03 GSE2	
110.00+03 ***	R ₂
3.5+06 GSE2	
3.6000+06 ***	R ₃
10.0000 GSE1	10%
432.0000 GSE2	
470.00+00 ***	R ₁
114.+03 GSE2	
120.00+03 ***	R ₂
3.5+06 GSE2	
3.3000+06 ***	R ₃
20.0000 GSE1	20%
432.0000 GSE2	
470.00+00 ***	R ₁
114.+03 GSE2	
100.00+03 ***	R ₂
3.5+06 GSE2	
3.3000+06 ***	R ₃

* Adapted from HP-65 Users' Library
program #00915A by Jacob Jacobs.

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01 *LBL1		50 X	10 EXP R7
02 1		51 R/S	*** R
03 2		52 *LBL8	Finds standard R
04 0		53 .	value from multiple
05 ÷		54 5	of step size
06 10*		55 +	Round up
07 ST02	10 ^{tol} /120	56 INT	
08 R/S		57 ST06	
09 *LBL2		58 2	
10 LOG		59 6	
11 ENT↑		60 X>Y?	
12 INT		61 GT06	
13 ST04		62 4	
14 -		63 7	
15 1		64 RCL6	
16 +		65 X>Y?	
17 10*		66 GT03	
18 ST03		67 1	26<R<47 then add 1
19 1		68 +	
20 ST-4		69 RTN	
21 1		70 *LBL3	
22 0		71 8	
23 ST05		72 3	
24 *LBL0		73 RCL6	
25 RCL3		74 X≠Y?	
26 RCL5	This step > Normal R?	75 RTN	
27 X>Y?		76 8	
28 GT09		77 2	
29 RCL2		78 RTN	
30 X		79 *LBL7	
31 ST05		80 RCL6	
32 GT00		81 ST07	
33 *LBL9		82 RTN	
34 GSB8		83 *LBL6	
35 ST07	This step	84 RCL6	
36 RCL5		85 RTN	
37 RCL2		86 R/S	
38 =			
39 GSB8			
40 ST06	Last step		
41 RCL7			
42 X		*** "Printx" may be inserted.	
43 IX			
44 RCL3	$\sqrt{(\text{This step}) \times (\text{Last step})}$		
45 X≠Y?			
46 GSB7			
47 RCL7			
48 RCL4			
49 10*			

REGISTERS

0	1	2 Step size	3 Normal R	4 Exp of R	5 This step
6 Temp	7 Temp	8	9	.0	.1
.2	.3	.4	.5	16	17
18	19	20	21	22	23
24	25	26	27	28	29

SMITH CHART CONVERSIONS

This program allows conversion among standing wave ratio, reflection coefficient, and return.

The parameters

σ = voltage standing wave ration

SWR = standing wave ratio expressed in decibels

ρ = reflection coefficient

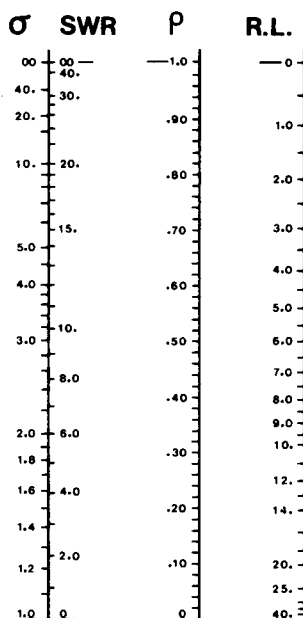
R.L. = return loss

are related as follows:

$$SWR = 20 \log \sigma$$

$$R.L. = 20 \log \frac{1}{\rho}$$

$$\sigma = \frac{1 + \rho}{1 - \rho}$$



The program also converts between impedance and reflection coefficient using the following relationships:

$$\Gamma = \rho \angle \phi = \frac{\frac{Z}{Z_0} - 1}{\frac{Z}{Z_0} + 1}$$

and

$$Z = Z \angle \theta = Z_0 \frac{1 + \Gamma}{1 - \Gamma}$$

where

Γ = complex reflection coefficient

$$\rho = |\Gamma|$$

$$\phi = \angle \Gamma$$

Z = impedance

$$Z = |Z|$$

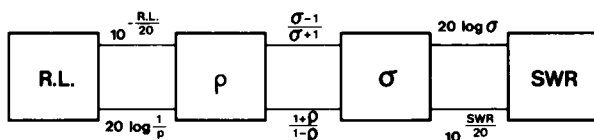
$$\theta = \angle Z$$

Z_0 = characteristic impedance

EXAMPLES:

1. Convert a 6 dB SWR to σ .
2. Convert a 7 dB return loss to SWR
3. A 50Ω system is terminated with an impedance of $62\angle 37^\circ$. What is the reflection coefficient?
4. A reflection coefficient of $.5\angle 7^\circ$ is observed in a 72Ω system. What is the impedance?

These relationships are perhaps more clearly seen in this sketch:



SOLUTIONS:

6.00 GSB4	R/S
2.00 *** σ	70.19 *** ϕ
7.00 GSB3	
GSB6	
GSB2	
8.75 *** SWR	72.00 ST01
	7.00 ENT↑
	0.50 GSB7
50.00 ST01	212.50 *** Z
37.00 ENT↑	R/S
62.00 GSB8	9.23 *** θ
0.75 *** ρ	

User Instructions

STEP	INSTRUCTIONS	INPUT DATA/UNITS	KEYS		OUTPUT DATA/UNITS
1.	Key in the program and choose an appropriate display format				
2.	Convert among σ , SWR, ρ , and R.L. as desired.				
	$\sigma \rightarrow$ SWR	σ	GSB	2	SWR
	SWR $\rightarrow \sigma$	SWR	GSB	4	σ
	$\sigma \rightarrow \rho$	σ	GSB	5	ρ
	$\rho \rightarrow \sigma$	ρ	GSB	6	σ
	$\rho \rightarrow$ R.L.	ρ	GSB	1	R.L.
	R.L. $\rightarrow \rho$	R.L.	GSB	3	ρ
3.	Store characteristic impedance	Z_0	ST0	1	
4.	Convert between Z and Γ as desired.				
	Z $\rightarrow \Gamma$	θ	ENT		
		Z	GSB	8	ρ
			R/S		ϕ
		ϕ	ENT		
	$\Gamma \rightarrow Z$	ϕ	GSB	7	Z
			R/S		θ

Program Listings

01 *LBL1	$\rho \rightarrow R.L.$	50 R/S	*** ϕ
02 1/X	$\sigma \rightarrow SWR$	51 *LBL0	$ \angle$
03 *LBL2		52 $\rightarrow R$	Re Im
04 LOG		53 ST04	
05 2		54 X $\div$ Y	
06 0		55 ST03	
07 x		56 X $\div$ Y	
08 R/S	*** R.L. or SWR	57 RCL5	
09 *LBL3	R.L. $\rightarrow \rho$	58 ST-4	Add in rectangular
10 CHS		59 +	form
11 *LBL4	SWR $\rightarrow \sigma$	60 $\rightarrow P$	$ 1 \angle 1$
12 2		61 ST02	
13 0		62 R↓	
14 ÷		63 RCL3	
15 10 ^x		64 RCL4	
16 R/S	*** ρ or σ	65 $\rightarrow P$	$ 2 \angle 2$
17 *LBL5	$\sigma \rightarrow \rho$	66 ST=2	Divide in polar
18 1/X		67 R↓	form
19 CHS		68 -	$\angle '$
20 *LBL6		69 RCL2	$ '$
21 1		70 RTN	
22 X $\div$ Y			
23 +			
24 1			
25 LSTX			
26 -			
27 ÷			
28 R/S	*** ρ or σ		
29 *LBL7	$\Gamma \rightarrow Z$		
30 1			
31 ST05			
32 R↓			
33 GSB0			
34 RCL1			
35 CHS			
36 x	Reverse $\angle$		
37 $\rightarrow R$			
38 $\rightarrow P$	*** Z		
39 R/S			
40 X $\div$ Y			
41 R/S	*** θ		
42 *LBL8	Z $\rightarrow \Gamma$		
43 RCL1			
44 CHS			
45 ST05			
46 R↓			
47 GSB0			
48 R/S			
49 X $\div$ Y	*** ρ		

REGISTERS

0	1 Z_0	2 $ 1 , '$	3 Im	4 Re, Re-k	5 k
6	7	8	9	.0	.1
.2	.3	.4	.5	16	17
18	19	20	21	22	23
24	25	26	27	28	29

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