

Hewlett-Packard HP-19C/HP-29C SOLUTIONS

NAVIGATION



INTRODUCTION

This HP-19C/HP-29C Solutions book was written to help you get the most from your calculator. The programs were chosen to provide useful calculations for many of the common problems encountered.

They will provide you with immediate capabilities in your everyday calculations and you will find them useful as guides to programming techniques for writing your own customized software. The comments on each program listing describe the approach used to reach the solution and help you follow the programmer's logic as you become an expert on your HP calculator.

You will find general information on how to key in and run programs under "A Word about Program Usage" in the Applications book you received with your calculator.

We hope that this Solutions book will be a valuable tool in your work and would appreciate your comments about it.

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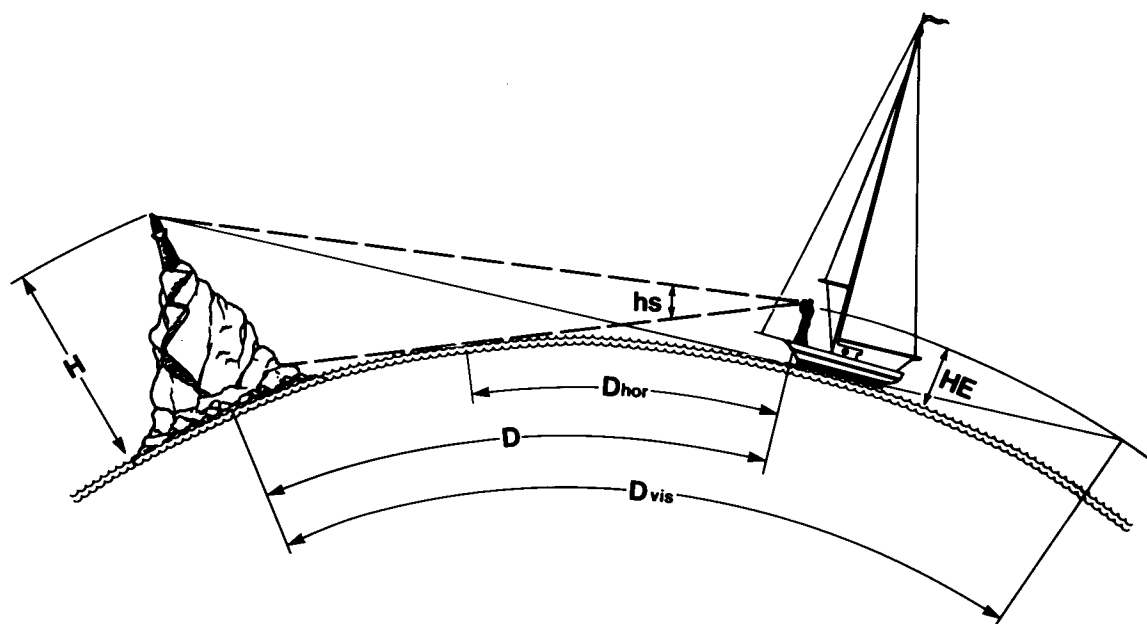
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* THIS PROGRAM ALSO APPEARS IN THE HP-19C/29C APPLICATIONS BOOK. IT HAS BEEN INCLUDED HERE, IN SLIGHTLY MODIFIED FORM, FOR THE SAKE OF COMPLETENESS.

DISTANCE TO OR BEYOND HORIZON



This program computes the distance to an object of known height whose base is obscured by the horizon and whose top subtends a sextant altitude hs with the horizon. The sextant altitude is corrected for index error and height of eye. Additional features are the calculation of the distance to the horizon for a given height of eye and the distance of visibility of an object of height H above sea level.

EQUATIONS:

$$D = \sqrt{\left(\frac{\tan h_a}{2.46 \times 10^{-4}}\right)^2 + \frac{H-HE}{0.74736}} - \frac{\tan h_a}{2.46 \times 10^{-4}}$$

$$D_{hor} = 1.144 \sqrt{HE}$$

$$D_{vis} = 1.144 (\sqrt{HE} + \sqrt{H})$$

where

D = distance to object, nautical miles

D_{hor} = distance to horizon, nautical miles

D_{vis} = distance of visibility, naut. miles

H = height of object beyond horizon, feet

HE = height of eye, feet

$h_a = hs + IC - 0.97 \sqrt{HE}$

hs = sextant altitude, D.MS

IC = index correction, M.m

EXAMPLE 1:

The height of eye of of an observer is 9 feet above sea level, how far away is his horizon?

EXAMPLE 2:

An observer "bobs" Farallon Light on the horizon and finds his height of eye to be 16 feet. The light is 358 feet above sea level. How far is the observer from the light? (Accuracy is affected by abnormal refraction)

EXAMPLE 3:

The top of a lighthouse, whose base is obscured by the horizon, is known to be 300 feet above sea level. It is found to have a sextant altitude of 25!6 above the horizon. The height of eye is 20 feet and the sextant requires an index correction of +1!3.

What is the distance to the lighthouse?

What is the distance to the horizon?

It has been determined that the luminous range of the light is "strong", now compute its visibility for the given height of eye.

SOLUTIONS:

(1)

9.00 ST02
GSB2
3.43 *** n.m.

(2)

16.00 ST02
358.00 ST03
GSB2
R/S
26.22 *** n.m.

(3)

1.30 ST01
20.00 ST02
300.00 ST03
0.2536 GSB1
6.28 *** n.m.
GSB2
5.12 *** n.m.
R/S
24.93 *** n.m.

User Instructions

[illegible]

Program Listings

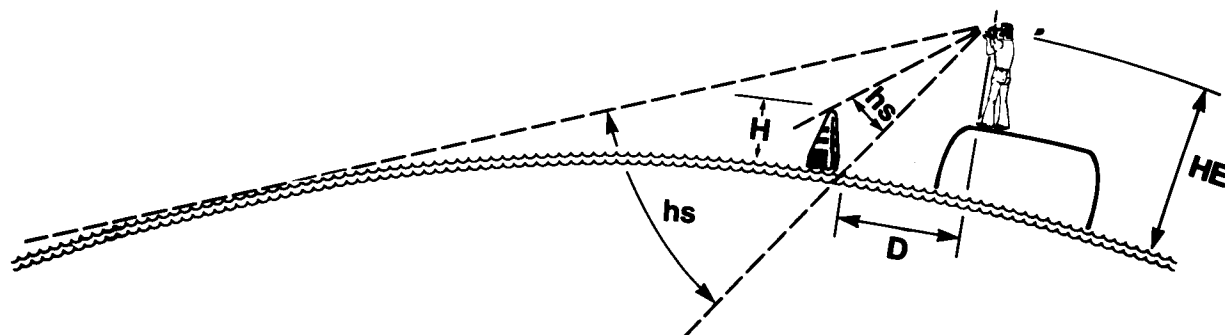
01 #LBL1	hs(D.MS)	48 x	1.144
02 +H	hs°	49 LSTX	
03 RCL1		50 RCL2	
04 RCL2		51 JX	
05 JX		52 x	
06 .		53 R/S	*** D _{hor}
07 9		54 +	** D _{vis}
08 7		55 R/S	
09 x			
10 -			
11 6			
12 0			
13 ÷			
14 +	ha°		
15 TAN			
16 2			
17 .			
18 4			
19 6			
20 EEX			
21 CHS			
22 4			
23 ÷			
24 STOS			
25 RCL3			
26 RCL2			
27 -			
28 .			
29 7			
30 4			
31 7			
32 3			
33 6			
34 ÷			
35 JX			
36 +P	$\sqrt{x^2 + y^2}$		
37 RCL5			
38 -			
39 R/S	** D		
40 #LBL2			
41 RCL3			
42 JX			
43 1			
44 .			
45 1			
46 4			
47 4			

** "Printx" may be inserted before "R/S".
 *** "Printx" may be used to replace
 "R/S".

REGISTERS

0	1 IC	2 HE	3 H	4	5 Used
6	7	8	9	.0	.1
.2	.3	.4	.5	16	17
18	19	20	21	22	23
24	25	26	27	28	29

DISTANCE BY HORIZON ANGLE AND DISTANCE SHORT OF HORIZON



This program calculates the distance between an observer and an object when (1) the vertical angle between its waterline and the horizon has been observed from a known height of eye or (2) the object's height is known, together with its subtended angle.

This program also calculates the height of an object if its subtended angle and distance from the observer are known.

EQUATIONS:

$$D = \frac{HE}{\tan(hs + IC + .97 \sqrt{HE})}$$

$$D = \frac{H}{\tan(hs + IC)}$$

where

D = distance to object, feet

HE= height of eye, feet

IC= index correction, M.m

H = height of object, feet

hs= sextant altitude, D.MS

NOTE:

hs < 10' may make D unreliable due to atmospheric conditions when vertical sextant altitude between object and horizon is taken.

EXAMPLE 1:

The sextant altitude between the waterline of a buoy and the horizon is found to be 21!4. The observer has a height of eye of 22 feet and the sextant requires a +1!7 index correction. How far is the observer from the buoy?

EXAMPLE 2:

The sextant altitude subtended by the base and the top of a 41 foot light tower is 56!2. The sextant requires a -1!9 index correction. How far is the observer from the light tower?

EXAMPLE 3:

A vessel is anchored 2015 feet from an observer. The sextant altitude between the vessel's waterline and truck of mast is 1°15!2. There is no index error. How high is the truck of the mast above the waterline?

SOLUTIONS:

(1)

1.70 ST01
22.00 ST02
0.2124 GSB1
2735.25 *** ft.
R/S
0.45 *** n.m.

(2)

-1.90 ST01
41.00 ENT↑
0.5612 GSB2
2595.50 *** ft.
R/S
0.43 *** n.m.

(3)

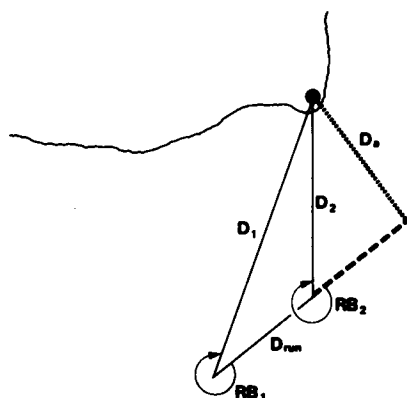
0.00 ST01
2015.00 ENT↑
1.1512 GSB3
44.08 *** ft.

Program Listings

01 *LBL1					
02 +H					
03 RCL1					
04 RCL2					
05 JX					
06 .					
07 9					
08 7					
09 x					
10 +					
11 GSB0					
12 RCL2					
13 X*Y					
14 ÷	D				
15 GT09					
16 *LBL2	hs H				
17 +H					
18 RCL1					
19 GSB0					
20 ÷					
21 *LBL9	D				
22 R/S	** D(ft.)				
23 6					
24 0					
25 7					
26 6					
27 ÷					
28 R/S	** D(n.m.)				
29 *LBL3	hs D(ft.)				
30 +H					
31 RCL1					
32 GSB0					
33 x					
34 R/S	** H (ft.)				
35 *LBL0					
36 6					
37 0					
38 ÷					
39 +					
40 TAN					
41 RTN					
** "Printx" may be inserted before "R/					
REGISTERS					
0	1 IC	2 HE	3	4	5
6	7	8	9	.0	.1
.2	.3	.4	.5	16	17
18	19	20	21	22	23
24	25	26	27	28	29

DISTANCE OFF AN OBJECT BY TWO BEARINGS

To determine the distance off an object as a vessel passes it, observe two bearings on the bow and note the distance run between bearings. The program calculates the distance off the object when it is abeam and at the time of the first and second bearings.



EQUATIONS:

$$D_2 = \frac{\sin RB_1}{\sin(RB_2 - RB_1)} D_{run}$$

$$D_{abeam} = |D_2 \sin RB_2|$$

$$D_1 = \left| \frac{D_{abeam}}{\sin RB_1} \right|$$

where

RB_1 = First relative bearing

RB_2 = Second relative bearing

D_{run} = St = Distance run

S = speed of vessel

t = time in minutes

D_1, D_2 = Distance at time of first or second bearing

D_a = Distance when abeam

EXAMPLE 1:

A lighthouse bears -026° (26° counter-clockwise) at 1130 and -051° at 1140. Our speed is 15 knots. How far will we be off the light when it is abeam? How far off were we at 1130 and 1140?

EXAMPLE 2:

A buoy is sighted bearing 015° on the bow, after a 3 mile run it bears 105° . What was its distance when abeam?

SOLUTIONS:

(1)

```

-26.00 ENT↑
-51.00 GSB1
15.00 ENT↑
0.10 GSB3
4.60 *** D1
    R↓
2.59 *** D2
    R↓
2.02 *** Dabeam
  
```

(2)

```

15.00 ENT↑
105.00 GSB1
3.00 GSB2
    R↓
    R↓
0.75 *** Dabeam
  
```


Program Listings

11

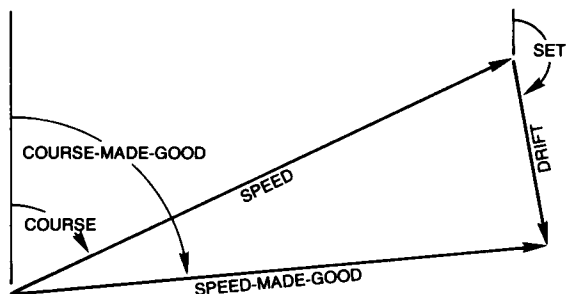
01 *LBL1	Store bearings t,s D _{run} D ₂ D _{abeam} D ₁ D ₁ , D ₂ , D _{abeam}			
02 ST02				
03 X*Y				
04 ST01				
05 R/S				
06 *LBL3				
07 →H				
08 x				
09 *LBL2				
10 RCL2				
11 RCL1				
12 -				
13 SIN				
14 ÷				
15 RCL1				
16 SIN				
17 x				
18 ST04				
19 RCL2				
20 SIN				
21 x				
22 ABS				
23 RCL4				
24 LSTX				
25 RCL1				
26 SIN				
27 ÷				
28 ABS				
29 R/S				

REGISTERS					
0	1 RB ₁	2 RB ₂	3	4 Used	5
6	7	8	9	.0	.1
.2	.3	.4	.5	16	17
18	19	20	21	22	23
24	25	26	27	28	29

VELOCITY TRIANGLE

This program is an interchangeable solution for the vector addition problem. Given any two of the vectors shown, the program computes the third.

SOLUTION:



```

5.00 ST01
20.50 ST02
60.00 ENT↑
2.00 GSB1
90.00 ENT↑
3.00 GSB3
      GSB5
1.02  ***   knots
      X=Y
98.86 ***   °T
  
```

Compass course is corrected on input for magnetic variation and deviation. True course is decorrected on output to yield compass course. Remember to update the values used for variation (changes with location) and deviation (changes with heading).

EXAMPLE:

A vessel is making 2 knots through the water, steering 060° by the compass. The magnetic variation is 20.5°E and the deviation is 5°E. Calculate the set and drift of the current if the vessel is making good 3 knots on a course of 090°T.

User Instructions

STEP	INSTRUCTIONS	INPUT DATA/UNITS	KEYS		OUTPUT DATA/UNITS
1.	Key in the program		<input type="text"/>	<input type="text"/>	
2.	Store compass corrections:		<input type="text"/>	<input type="text"/>	
	Deviation (negative if west)	$\pm Dev^\circ$	STO	1	
	Variation (negative if west)	$\pm Var^\circ$	STO	2	
3.	Enter any two of the three vectors:		<input type="text"/>	<input type="text"/>	
3a.	Heading -		<input type="text"/>	<input type="text"/>	
	Compass course	C_c°	ENT↑	<input type="text"/>	
	Speed	S, knots	GSB	1	
3b.	Current -		<input type="text"/>	<input type="text"/>	
	Set	Set $^\circ$	ENT↑	<input type="text"/>	
	Drift	Drift, knots	GSB	2	
3c.	Course -		<input type="text"/>	<input type="text"/>	
	Course made good	CMG $^\circ$	ENT↑	<input type="text"/>	
	Speed made good	SMG, knots	GSB	3	
4.	Compute the remaining vector:		<input type="text"/>	<input type="text"/>	
4a.	Heading -		<input type="text"/>	<input type="text"/>	
	Speed		GSB	4	S, knots
	Compass course		x↔y	<input type="text"/>	C_c°
	True course		RCL	4	C_t°
4b.	Current -		<input type="text"/>	<input type="text"/>	
	Drift		GSB	5	Drift/knots
	Set		x↔y	<input type="text"/>	Set $^\circ$
4c.	Course -		<input type="text"/>	<input type="text"/>	
	Speed made good		GSB	6	SMG, knots
	Course made good		x↔y	<input type="text"/>	CMG $^\circ$
			<input type="text"/>	<input type="text"/>	
			<input type="text"/>	<input type="text"/>	

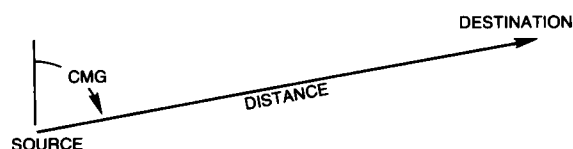
Program Listings

01 #LBL1	Enter heading	50 RCL5	
02 ST05		51 →R	X ₁ ,Y ₁
03 X↔Y		52 ST.0	
04 ST03		53 X↔Y	
05 RCL1		54 RCL8	
06 +		55 RCL9	
07 RCL2		56 GSB0	CMG
08 +		57 ST06	
09 GSB9	Normalize angle	58 X↔Y	
10 ST04		59 ST07	SMG
11 R/S		60 R/S	
12 #LBL2	Enter current	61 #LBL7	
13 ST09		62 RCL6	
14 X↔Y		63 RCL7	
15 ST08		64 →R	X ₁ ,Y ₁
16 R/S		65 ST.0	
17 #LBL3	Enter course	66 X↔Y	
18 ST07		67 RTN	
19 X↔Y		68 #LBL0	X ₂ ,Y ₂ ,Y ₁
20 ST06		69 →R	
21 R/S		70 S+.0	
22 #LBL4	Compute heading	71 R↓	
23 GSB7		72 +	
24 RCL8		73 RC.0	X ₁ +X ₂ ,Y ₁ +Y ₂
25 RCL9		74 →P	
26 CHS		75 X↔Y	
27 GSB0		76 GSB9	Normalize angle
28 ST04	C _t	77 RTN	
29 RCL1		78 #LBL9	
30 -		79 3	
31 RCL2		80 6	
32 -		81 0	
33 GSB9	Normalize angle	82 →R	
34 ST03	C _c	83 →P	
35 X↔Y		84 X↔Y	∠,360
36 ST05	Speed	85 X<0?	
37 R/S		86 GT08	
38 #LBL5	Compute current	87 X↔Y	
39 GSB7		88 R↓	∠
40 RCL4		89 RTN	
41 RCL5		90 #LBL8	
42 CHS		91 +	360 + ∠
43 GSB0		92 RTN	
44 ST08	Set		
45 X↔Y	Drift		
46 ST09			
47 R/S	Compute course		
48 #LBL6			
49 RCL4			

REGISTERS					
0	1 Dev	2 Var	3 C _c	4 C _t	5 Speed
6 CMG	7 SMG	8 Set	9 Drift	10 Used	11
12	13	14	15	16	17
18	19	20	21	22	23
24	25	26	27	28	29

COURSE TO STEER

This program calculates a course to steer given your location, the location where you want to go, your boat's speed through the water, and the set and drift of the current.



EXAMPLE:

A vessel making 6 knots through the water is at (45°N, 124°40'W) and she wishes to steer a course toward (44°40'N, 124°10'W). The magnetic variation is 20°5E and there is a 2 knot current setting 090°. What course should she steer.

SOLUTION:

```

0.00 ST01
20.50 ST02
90.00 ST08
2.00 ST09
45.00 ENT↑
124.40 ENT↑
44.40 ENT↑
124.10 GSB1
29.20 *** Dist., n.m.
6.00 GSB2
125.93 *** Course to steer,degrees
      R/S
7.30 *** Speed made good,knots
      R/S
4.00 *** Transit time, H.MS
  
```

[illegible]

Program Listings

17

01 *LBL1	$\lambda_2 L_2 \lambda_1 L_1$	50 ST07	
02 +H		51 GSB7	SMG, CMB
03 XZY	L_2	52 CHS	
04 +H		53 GSB0	
05 ST.1		54 RCL1	
06 R↓		55 -	
07 XZY	λ_1	56 RCL2	
08 +H		57 -	
09 -		58 GSB9	C_c
10 CHS	$\lambda_1' - \lambda_2'$	59 R/S	Dist
11 ST.2		60 RC.1	
12 R↓		61 RCL7	
13 +H	L_1	62 R/S	SMG (knots)
14 S-.1	$L_1 + L_2$	63 ÷	
15 +		64 +HMS	Time (H.MS)
16 2		65 R/S	Normalize:
17 ÷	Ang., latitude	66 *LBL9	$0 < \text{angle} < 360$
18 COS		67 3	
19 RC.2		68 6	
20 x		69 0	
21 RC.1	$\sqrt{x^2 + y^2}$	70 +R	
22 +P		71 +P	
23 6		72 XZY	
24 0	Convert to n.m.	73 X<0?	
25 x		74 GT08	
26 ST.1		75 XZY	
27 XZY		76 R↓	
28 GSB9		77 RTN	
29 ST06	CMG	78 *LBL8	
30 XZY		79 +	
31 R/S	Dist. (n.m.)	80 RTN	Vector add
32 *LBL2	Enter speed and	81 *LBL0	x_2, y_2
33 ST05	Compute C_c	82 +R	
34 RCL6		83 S+.0	
35 RCL8		84 R↓	
36 RCL6		85 +	
37 -		86 RC.0	$y_1 + y_2$
38 SIN		87 +P	$x_1 + x_2$
39 RCL9		88 XZY	r
40 x		89 GSB9	0
41 RCL5		90 RTN	0'
42 ÷		91 *LBL7	Vector add
43 SIN-		92 +R	x_1, y_1
44 -		93 ST.0	
45 GSB9	C_t	94 XZY	
46 RCL5		95 RCL8	
47 GSB7		96 RCL9	
48 GSB0		97 RTN	
49 XZY	SMG		

REGISTERS

0	1 Dev	2 Var	3	4	5 Speed
6 CMG	7 SMG	8 Set	9 Drift	10 Used	11 Used
12 Used	13	14	15	16	17
18	19	20	21	22	23
24	25	26	27	28	29

ESTIMATED TIME OF ARRIVAL

This program computes the time of arrival at the next port in local zone time and GMT, when distance, speed, departure date and time in local zone time are input.

It also computes speed required to make a given ETA, when distance, date and time of departure in local zone time and date and time of desired arrival in local zone time are input.

All computations can be made in GMT by storing zeros in registers 4 and 5 and entering GMT times.

EXAMPLES:

1. A vessel departs San Francisco at 0030 on the 2nd of January local time, bound for Guam, distance 5,146 miles. What will be the date and time of arrival Guam local time, and GMT at 15.5 knots.
2. If the same Vessel makes the same departure time and wishes to arrive in Guam at 0700 on the 16th of January local Guam time, what speed is required.

NOTE:

Zone time of San Francisco is +8 and Guam is -10.

REFERENCE:

This program is adapted from HP-65 Users' Library program #02185A by Capt. Kenneth R. Orcutt.

SOLUTIONS:

(1)	5146.00 ST01	
	15.50 ST02	
	8.00 ST04	
	-10.00 ST05	
	2.0030 GSB1	
	16.1430 ***	Local time
	R/S	
	16.0430 ***	GMT

(2)	2.0030 ENT1	
	16.0700 GSB2	
	15.8582 ***	Knots

Program Listings

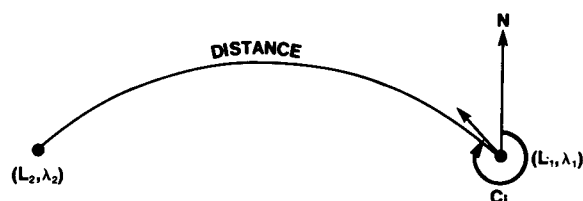
01 *LBL1	Compute arrival	50 +	
02 4		51 RTN	
03 ST00	i = 4	52 *LBL2	Arriv. time.Dep.
04 R↓		53 5	Time
05 GSB0		54 ST00	i = 5
06 RCL1		55 R↓	
07 RCL2		56 GSB0	
08 ÷	Time of transit	57 X*Y	Dep. time
09 RCL9		58 DSZ	i = 4
10 ÷		59 GSB0	
11 +		60 -	Total transit time
12 ST07	Add to departure	61 RCL1	
13 RCL5	time	62 X*Y	
14 RCL9		63 ÷	Speed
15 ÷		64 RCL9	
16 -	Arrival time	65 ÷	**
17 *LBL9		66 R/S	Speed, knots
18 INT	DD.		
19 LSTX			
20 FRC			
21 RCL9			
22 x	Convert to hours		
23 +HMS			
24 1			
25 0	Format display		
26 0			
27 ÷			
28 +	**		
29 R/S	Arrival time and		
30 RCL7	date, local and		
31 GT09	GMT		
32 *LBL0	Set display		
33 FIX4	DD.		
34 INT			
35 LSTX			
36 FRC			
37 1			
38 0			
39 0			
40 x			
41 +H			
42 2			
43 4			
44 ST09			
45 ÷	Add DD.		
46 +	Time zone		
47 RCLi			
48 RCL9			
49 ÷			

REGISTERS					
0 i	1 Distance	2 Speed	3	4 Dep. Time Zone	5 Arriv. TIME Zone
6	Used		24	.0	.1
.2	.3	.4	.5	16	17
18	19	20	21	22	23
24	25	26	27	28	29

** "PRINTX" may be inserted before "R/S".

GREAT CIRCLE NAVIGATION

This program calculates the great circle distance between two points and the initial course from the first point. Coordinates are input in degrees-minutes-seconds format. The distance is displayed in nautical miles and the initial course in decimal degrees.



EQUATIONS:

$$D = 60 \cos^{-1} [\sin L_1 \sin L_2 + \cos L_1 \cos L_2 \cos (\lambda_2 - \lambda_1)]$$

$$C = \cos^{-1} \left[\frac{\sin L_2 - \sin L_1 \cos (D/60)}{\sin (D/60) \cos L_1} \right]$$

$$C_i = \begin{cases} C; \sin (\lambda_2 - \lambda_1) < 0 \\ 360 - C; \sin (\lambda_2 - \lambda_1) \geq 0 \end{cases}$$

where:

L_1, λ_1 = coordinates of initial point

L_2, λ_2 = coordinates of final point

D = distance from initial to final point

C_i = initial course from initial to final point

REMARKS:

- Southern latitudes and eastern longitudes must be entered as negative numbers.
- Truncation and round off errors occur when the source and destination are very close together (1 mile or less).

- Do not use coordinates located at diametrically opposite sides of the earth.
- Do not use latitudes of $+90^\circ$ or -90° .
- Do not try to compute initial heading along a line of longitude ($L_1=L_2$).
- This program assumes the calculator is set in DEG mode.

EXAMPLE 1:

Find the distance and initial course for the great circle from Tokyo ($L35^\circ40'N$, $\lambda139^\circ45'E$) to San Francisco ($L37^\circ49'N$, $\lambda122^\circ25'W$).

EXAMPLE 2:

What is the distance and initial great circle course from $L33^\circ53'30''S$, $\lambda18^\circ23'10''E$ to $L40^\circ27'10''N$, $\lambda73^\circ49'40''W$?

SOLUTIONS:

- (1)
- ```

35.40 ENT↑
-139.45 ENT↑
37.49 ENT↑
122.25 GSB1
4460.04 *** (D,n.m)
R/S
54.37 *** (Ci,dec.deg.)

```
- (2)
- ```

-33.5330 ENT↑
-18.2310 ENT↑
40.2710 ENT↑
73.4940 GSB1
6763.09 *** (D,n.m.)
R/S
304.48 *** (Ci,dec.deg.)

```

[illegible]

Program Listings

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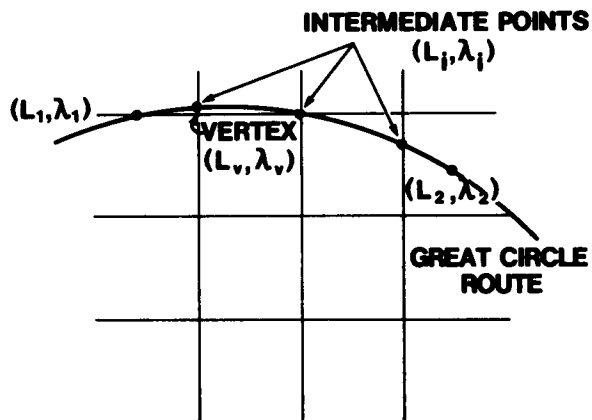
01 *LBL1		48 SIN	
02 +H		49 ÷	
03 ST03		50 COS-	C
04 R↓		51 RCL0	
05 +H		52 SIN	
06 ST01		53 X<0?	
07 R↓		54 GT09	
08 +H		55 R↓	
09 ST04		56 3	
10 R↓		57 6	
11 +H		58 0	
12 ST02		59 X≠Y	
13 RCL2		60 -	** C _i
14 SIN		61 RTN	
15 RCL1		62 *LBL9	
16 SIN		63 R↓	
17 X		64 RTN	** C _i
18 RCL2			
19 COS			
20 RCL1			
21 COS			
22 X			
23 RCL3			
24 RCL4			
25 -			
26 ST00			
27 COS			
28 X			
29 +			
30 ST05			
31 COS-			
32 ST06			
33 6			
34 0			
35 X			
36 R/S	** D		
37 RCL1			
38 SIN		** "Printx" may be inserted before "R/S" and "RTN".	
39 RCL2			
40 SIN			
41 RCL5			
42 X			
43 -			
44 RCL2			
45 COS			
46 ÷			
47 RCL6			

REGISTERS

0 $\lambda_2 - \lambda_1$	1 L_2	2 L_1	3 λ_2	4 λ_1	5 COS D/60
6	7	8	9	10	11
12	13	14	15	16	17
18	19	20	21	22	23
24	25	26	27	28	29

GREAT CIRCLE COMPUTATION

This program computes the latitude corresponding to a specified longitude on a great circle passing through two given points.



EQUATIONS:

$$L_i = \tan^{-1} \left[\frac{\tan L_2 \sin(\lambda_i - \lambda_1) - \tan L_1 \sin(\lambda_i - \lambda_2)}{\sin(\lambda_2 - \lambda_1)} \right]$$

where

(L_1, λ_1) = coordinates of initial point

(L_2, λ_2) = coordinates of final point

(L_i, λ_i) = coordinates of intermediate point

NOTES:

The program does not compute along lines of longitude ($\lambda_1 = \lambda_2$).

EXAMPLE:

A ship is proceeding from Manila to Los Angeles. The captain wishes to use great-circle sailing from $L12^\circ45'2N$, $\lambda124^\circ20'1E$, off the entrance to San Bernardino Strait, to $L33^\circ48'8N$, $\lambda120^\circ07'1W$, five miles south of Santa Rosa Island. Find the latitudes corresponding to 1) $\lambda = 160^\circ34'W$; and 2) $\lambda = 180^\circ$.

SOLUTION:

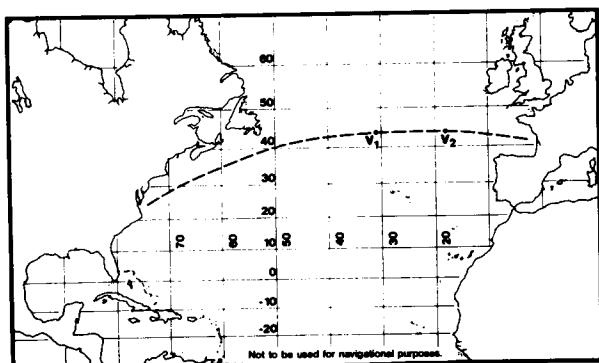
```

12.4512 ENT↑
-124.2006 ENT↑
33.4848 ENT↑
120.0706 GSB1
160.3400 GSB2
41.2108 *** °N
180.0000 GSB2
39.4133 *** °N

```


COMPOSITE SAILING

When the great circle would carry a vessel to a higher latitude than desired, a modification of great-circle sailing, called composite sailing, may be used to good advantage. The composite track consists of a great circle from the point of departure and tangent to the limiting parallel, a course line along the parallel, and a great circle tangent to the limiting parallel and through the destination. This program computes, for each of two points, the longitude at which a great circle through the point is tangent to some limiting parallel.



EQUATIONS:

$$\lambda_{V1} = \lambda_1 + \cos^{-1} \left(\frac{\tan L_1}{\tan L_{\max}} \right) S_1 S_2$$

$$\lambda_{V2} = \lambda_2 + \cos^{-1} \left(\frac{\tan L_2}{\tan L_{\max}} \right) S_3 S_2$$

where

(L_1, λ_1) = initial position

(L_2, λ_2) = final position

(L_{\max}, λ_{V1}) = point at which limiting parallel is met

(L_{\max}, λ_{V2}) = point at which limiting parallel is left

$$S_1 = \text{sgn} (\lambda_2 - \lambda_1)$$

$$S_2 = \text{sgn} (|\lambda_2 - \lambda_1| - 180)$$

$$S_3 = -S_1$$

$$\text{sgn}(x) = \begin{cases} +1 & ; x \geq 0 \\ -1 & ; x < 0 \end{cases}$$

EXAMPLE:

A ship leaves Baltimore bound for Bordeaux (Royan), France. The captain desires to use composite sailing from $L36^\circ 57' 7''N$, $\lambda 75^\circ 42' 2''W$ one mile south of Chesapeake Light to $L45^\circ 39' 1''N$, $\lambda 1^\circ 29' 8''W$, near the entrance to Grande Passe de l'Quest, limiting the maximum latitude to $47^\circ N$.

Required:

- (1) The longitude at which the limiting parallel is reached.
- (2) The longitude at which the limiting parallel should be left.

SOLUTION:

```

36.5742 ENT↑
75.4212 ENT↑
45.3906 ENT↑
 1.2948 GSB1
47.0000 GSB2
30.1607 *** λV1 (D.MS)
      R/S
18.5653 *** λV2 (D.MS)
  
```

User Instructions

[illegible]

Program Listings

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<div>01 *LBL1</div> <div>02 +H</div> <div>03 ST03</div> <div>04 R↓</div> <div>05 +H</div> <div>06 ST01</div> <div>07 R↓</div> <div>08 +H</div> <div>09 ST04</div> <div>10 R↓</div> <div>11 +H</div> <div>12 ST02</div> <div>13 R/S</div> <div>14 *LBL2</div> <div>15 TAN</div> <div>16 ST05</div> <div>17 RCL2</div> <div>18 TAN</div> <div>19 X↔Y</div> <div>20 ÷</div> <div>21 COS⁻¹</div> <div>22 RCL3</div> <div>23 RCL4</div> <div>24 -</div> <div>25 ENT↑</div> <div>26 ABS</div> <div>27 1</div> <div>28 8</div> <div>29 0</div> <div>30 -</div> <div>31 x</div> <div>32 ENT↑</div> <div>33 ABS</div> <div>34 ÷</div> <div>35 ST06</div> <div>36 CHS</div> <div>37 x</div> <div>38 RCL4</div> <div>39 *LBL0</div> <div>40 +</div> <div>41 1</div> <div>42 +R</div> <div>43 +P</div> <div>44 X↔Y</div> <div>45 +HMS</div> <div>46 R/S</div> <div>47 RCL1</div> <div>48 TAN</div> <div>49 RCL5</div>	<div>$\lambda_2 \quad L_2 \quad \lambda_1 \quad L_1$</div> <div>Enter L_{\max}</div> <div>$\lambda_2 - \lambda_1$</div> <div>$\lambda_2 - \lambda_1 \quad \lambda_2 - \lambda_1$</div> <div>$\pm 1$</div> <div>Normalize Angle</div> <div>$** \lambda_{V1}, \lambda_{V2}$</div>	<div>50 ÷</div> <div>51 COS⁻¹</div> <div>52 RCL6</div> <div>53 x</div> <div>54 RCL3</div> <div>55 GT00</div>	<div>sgn</div> <div>** "PRINTX" may be inserted before "R/S".</div>		
REGISTERS					
0	1 L_2	2 L_1	3 λ_2	4 λ_1	5 $\tan L_{\max}$
6 sgn	7	8	9	0	1
2	3	4	5	16	17
18	19	20	21	22	23
24	25	26	27	28	29

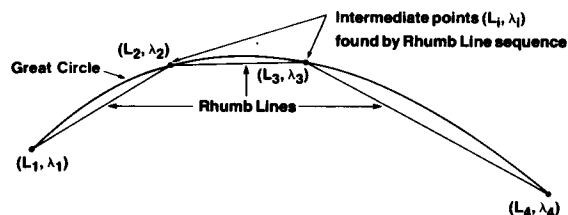
RHUMB LINE NAVIGATION

This program is designed to assist in the activity of course planning. You supply the latitude and longitude of the point or origin and the destination. The program calculates the rhumb line course and the distance from origin to the destination.

Since the rhumb line is the constant-course path between points on the globe, it forms the basis of short distance navigation. In low and midlatitudes the rhumb line is sufficient for virtually all course and distance calculations which navigators encounter. However, as distance increases or at high latitudes the rhumb line ceases to be an efficient track since it is not the shortest distance between points.

The shortest distance between points on a sphere is the great circle. However, in order to steam great circles, an infinite number of course changes are necessary. Since it is impossible to calculate an infinite number of courses at an infinite number of points, several rhumb lines may be used to approximate a great circle. The more rhumb lines used the closer to the great circle distance the sum of the rhumb line distances will be. The Great Circle Computation program may be used to calculate intermediate course change points which can be linked by rhumb lines.

Latitudes and longitudes are input in degrees-minutes-seconds. Course is displayed in decimal degrees. Southern latitudes and eastern longitudes are input as negative numbers.



EQUATIONS:

$$C = \tan^{-1} \frac{\pi (\lambda_1 - \lambda_2)}{180 (\ln \tan (45 + \frac{1}{2} L_2) - \ln \tan (45 + \frac{1}{2} L_1))}$$

$$D = \begin{cases} 60 (\lambda_2 - \lambda_1) \cos L; \cos C = 0 \\ 60 \frac{(L_2 - L_1)}{\cos C}; \text{otherwise} \end{cases}$$

where:

(L_1, λ_1) = position of initial point

(L_2, λ_2) = position of final point

D = rhumb line distance

C = rhumb line course

REMARKS:

- No course should pass through either the south or north pole.
- Errors in distance calculations may be encountered as $\cos C$ approaches zero.
- Accuracy deteriorates for very short legs.
- This program assumes the calculator is set in DEG mode.

EXAMPLE 1:

What is the distance and course from
 $L35^{\circ}24'12''N, \lambda 125^{\circ}02'36''W$ to $L41^{\circ}09'12''N,$
 $\lambda 147^{\circ}22'36''E$?

EXAMPLE 2:

What course should be sailed to travel
 a rhumb line from $L2^{\circ}13'42''S,$
 $\lambda 179^{\circ}07'54''E$ to $L5^{\circ}27'24''N,$
 $\lambda 179^{\circ}24'36''W$? What is the distance?

SOLUTIONS:

(1) 35.2412 ENT↑
 125.0236 ENT↑
 41.0912 ENT↑
 -147.2236 GSB1
 4135.60 *** (DIST., n.m.)
 R/S
 274.79 *** (C, dec, deg.)

(2) +
 -2.1342 ENT↑
 -179.0754 ENT↑
 5.2724 ENT↑
 179.2436 GSB1
 469.31 *** (DIST., n.m.)
 R/S
 10.73 *** (C, dec, deg.)

[illegible]

Program Listings

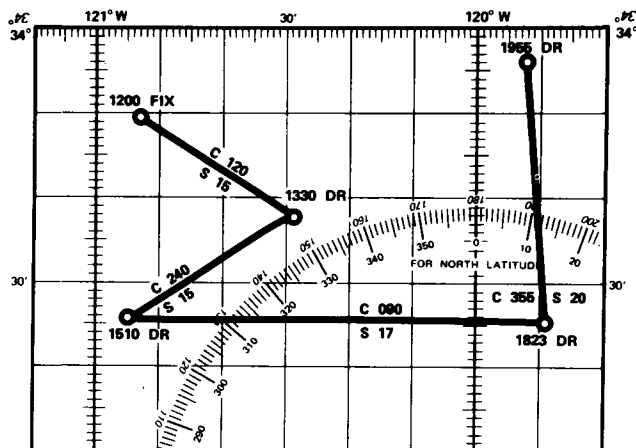
33

01 *LBL1		48 LN	
02 +H		49 RTN	
03 ST03	λ_2	50 *LBL8	
04 R↓		51 3	
05 +H		52 6	E to W 360 - C
06 ST01	L_2	53 0	
07 R↓		54 RCL5	
08 +H	λ_1	55 ABS	
09 ST04		56 -	
10 R↓		57 *LBL7	
11 +H		58 ABS	
12 ST02	L_1	59 ST06	
13 RCL4	$\lambda_1 - \lambda_2$	60 1	
14 RCL3		61 8	
15 -		62 0	
16 ST00		63 RCL0	
17 2	Make $-180 < \lambda_1 - \lambda_2$	64 ABS	
18 ÷	< 180	65 X<Y?	is $[\lambda_1 - \lambda_2] > 180^\circ$
19 SIN		66 GSB6	If so subtract from
20 SIN-		67 RCL1	360
21 9		68 COS	
22 0		69 x	
23 ÷		70 ST07	
24 P↓		71 RCL1	
25 x		72 RCL2	
26 RCL1		73 -	
27 GSB9		74 RCL5	
28 RCL2		75 COS	
29 GSB9		76 X#0?	is C = 90°?
30 -		77 ÷	
31 +P		78 ENT↑	
32 R↓		79 X=0?	
33 ST05	C	80 RCL7	
34 RCL0		81 6	
35 SIN		82 0	
36 SIN-		83 x	
37 X<0?	x<0 means east to	84 ABS	** Distance
38 GT08	west	85 R/S	** Course
39 RCL5		86 RCL6	
40 GT07		87 RTN	
41 *LBL9	If west to east	88 *LBL6	
42 2	C is answer	89 3	
43 ÷		90 6	If $[\lambda_1 - \lambda_2] > 180^\circ$
44 4		91 0	
45 5		92 X#Y	
46 +		93 -	
47 TAN		94 RTN	
		95 R/S	then $360 - [\lambda_1 - \lambda_2]$

REGISTERS

0 $\lambda_1 - \lambda_2$	1 L_2	2 L_1	3 λ_2	4 λ_1	5 Used
6	7	8	9	.0	.1
.2	** "Printx" may be inserted before "R/S" & "RTN".				17
18	19	20	21	22	23
24	25	26	27	28	29

RHUMB LINE DEAD RECKONING



This program calculates a ship's DR position given the ship's course, speed, and elapsed time from the last fix or DR position. The DR position is stored so that on subsequent legs just course, speed, and elapsed time need be entered to obtain the updated DR position. The program may be used for both small and large area DR problems.

EQUATIONS:

The updated position (L, λ) is given by following a loxodrome (rhumb line) from the initial position (L_i, λ_i) for a distance determined by the speed and time.

$$L = L_i + \Delta t \frac{S \cos C}{60}$$

$$\lambda = \begin{cases} \lambda_i + \frac{180 \tan C (\tan(45 + \frac{L_i}{2}) - \tan(45 + \frac{L}{2}))}{\pi} ; & C \neq 90 \text{ or } 270 (L_i \neq L) \\ \lambda_i - \Delta t \frac{S \sin C}{60 \cos L_i} ; & C = 90 \text{ or } 270 (L_i = L) \end{cases}$$

where:

- L_i = initial latitude (N, positive; S, negative)
- L = updated latitude
- λ_i = initial longitude (W, positive; S, negative)
- λ = updated longitude
- S = ship's speed, knots
- C = ship's course, degrees
- Δt = the time (H.MS) between initial and final positions.

NOTES:

1. The program cannot follow a meridian over a pole.
2. The program loses accuracy and gets incorrect answers when within 0.5° of a pole.

EXAMPLE (Fig. 1):

A vessel's position is $L33^\circ49'11''N$, $\lambda120^\circ52'00''W$ at 1200. If she steams as shown, what is her position at each time?

TIME	C	S	DR
1200			$L33^\circ49'06''N, \lambda120^\circ52'00''W$
1330	120°	15 knots	$(L33^\circ37'51''N, \lambda120^\circ28'34''W)$
1510	240°	15 knots	$(L33^\circ25'21''N, \lambda120^\circ54'32''W)$
1823	90°	17 knots	$(L33^\circ25'21''N, \lambda119^\circ49'01''W)$
1955	355°	20 knots	$(L33^\circ55'54''N, \lambda119^\circ52'14''W)$

SOLUTION:

33.4906	ENT↑	
120.5200	GSB1	
13.3000	ENT↑	
12.0000	GSB3	
120.0000	ENT↑	
15.0000	GSB2	
33.3751	***	
	R/S	1330 DR
120.2834	***	
15.1000	ENT↑	
13.3000	GSB3	
240.0000	ENT↑	
15.0000	GSB2	
33.2521	***	
	R/S	1510 DR
120.5433	***	
18.2300	ENT↑	
15.1000	GSB3	
90.0000	ENT↑	
17.0000	GSB2	
33.2521	***	
	R/S	1823 DR
119.4902	***	
19.5500	ENT↑	
18.2300	GSB3	
355.0000	ENT↑	
20.0000	GSB2	
33.5554	***	
	R/S	1955 DR
119.5214	***	

Program Listings

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01 #LBL1	$\lambda_1 L_1$	50 ST02	λ
02 FIX4		51 RCL1	
03 +H		52 +HMS	*** L
04 ST02		53 R/S	
05 X \leftrightarrow Y		54 RCL2	
06 +H		55 +HMS	** λ
07 ST01		56 R/S	
08 R/S		57 #LBL0	
09 #LBL2	S C Δt	58 9	
10 +R	ScosC	59 0	
11 ST05	SsinC	60 +	
12 R \downarrow		61 2	
13 ST06		62 \div	
14 R \downarrow		63 TAN	
15 +H		64 RTN	
16 ST07		65 #LBL9	
17 RCL5		66 RCL6	
18 x		67 RCL7	
19 6		68 x	
20 0		69 RCL1	
21 \div		70 COS	
22 RCL1	L_i	71 6	
23 +	L	72 0	
24 ST01	L_i	73 x	
25 LSTX	C = 90° or 270°	74 CHS	
26 X=Y?		75 GT08	Δt routine
27 GT09		76 #LBL3	
28 GSB0		77 +H	
29 RCL1		78 X \leftrightarrow Y	
30 GSB0		79 +H	
31 \div		80 -	
32 LN		81 ABS	
33 RCL6		82 +HMS	** Δt
34 x		83 R/S	
35 RCL5			
36 \div			
37 1			
38 0			
39 0			
40 x			
41 P \downarrow			
42 #LBL8			
43 \div			
44 RCL2	λ_i		
45 +			
46 1			
47 +R	Normalize		
48 +P	Angle		
49 X \leftrightarrow Y			
** "PRINTX" may be inserted before "R/"			
*** "PRINTX" may be used to replace "R/"			

REGISTERS					
0	1 L	2 λ	3	4	5 ScosC
6 SsinC	7 Δt	8	9	10 .0	11 .1
12	13	14	15	16	17
18	19	20	21	22	23
24	25	26	27	28	29

** "PRINTX" may be inserted before "R/S".
 *** "PRINTX" may be used to replace "R/S".

CELESTIAL NAVIGATION AND DEAD RECKONING

This program allows you to update a vessel's position and correct it using sights on a celestial object. The program is started with your latitude and longitude and the object's GHA and declination all determined for the same time. Then when any other time is keyed in, the corresponding DR is computed. If a sight is taken at that time, the resulting altitude may be entered into the calculator to yield an intercept and azimuth. The DR may be moved accordingly if desired.

The dead reckoning technique used is mid-latitude sailing which, while not as accurate as rhumb line dead reckoning, is sufficiently good for most purposes. Altitude intercepts "toward" are considered to be positive, even though careful reading of Bowditch would indicate the opposite. By using this convention, it is easy to compute the intercept terminus (most probable position or MPP).

The program contains a useful subroutine, GSB 7, which can be used for translating almanac entries in degrees, minutes and tenths (DM.M) to decimal degrees (D.d).

REFERENCE:

This program is based on private communications with Paul E. Shaad of Sacramento, California.

EXAMPLE:

On February 19, 1975, a ship is steaming on course 240 at 17 knots. At 1800 GMT her dead reckoning position is 42°N, 135°W. Compute her position at 2115.

Her navigator shoots the Sun from a height of 65' (dip = 7'8"). At 2340 he obtains a sextant altitude of 28°25'36". Compute the altitude intercept and azimuth and correct the ship's DR.

SOLUTION

From The Nautical Almanac we take the Sun's GHA and declination at 1800 and 1900 GMT and also the Sun's semidiameter.

G.M.T.	SUN			
	G.H.A.		Dec.	
d h	°	'	°	'
19 18	86	31.5	S11	18.5
19	101	31.5		17.6

S.D. 16.2		
8631.5000 GSB7	GHA at 1800	
86.5250 ***		
ST01		
-1118.5000 GSB7	DEC at 1800	
-11.3083 ***		
ST02		
16.2000 GSB7	Semidiameter	
0.2700 ***		
ST03		
42.0000 ST04	Lat.	} Position at 1800
135.0000 ST05	Long.	
7.8000 GSB7	Dip of the horizon	
0.1300 ***		
ST06		
240.0000 ST07	Course	
17.0000 ENT↑	Speed	
60.0000 ÷		
0.2833 ***	Speed converted to degrees per hour	
ST08		
18.0000 ST09	Time	
10131.5000 GSB7		
101.5250 ***	} Calculation of Rate of Change of GHA	
8631.5000 GSB7		
86.5250 ***		
-		
15.0000 ***		
ST.1		
-1117.6000 GSB7	} Calculation of Rate of Change of DEC	
-11.2933 ***		
-1118.5000 GSB7		
-11.3083 ***		
-		
0.0150 ***		
ST.2		

Now that the setup is complete, you can dead reckon and reduce sights all day long.

21.1500	GSB1	New time	
41.3223	***	Latitude	} New Position at 2115
	X*Y		
136.0409	***	Longitude	

23.4000	GSB1	New time	
41.1150	***	Latitude	} New Position at 2340
	X*Y		
136.5134	***	Longitude	
28.2536	GSB2	Sextant altitude	
-4.3689	***	Altitude intercept	
	X*Y		
219.4574	***	Azimuth	
	X*Y		
	GSB7		
-0.0728	***	Intercept converted to degrees	
	GSB3		
41.1512	***	Latitude	} Intercept terminus on Line of Position
	X*Y		
136.4752	***	Longitude	

User Instructions

STEP	INSTRUCTIONS	INPUT DATA/UNITS	KEYS		OUTPUT DATA/UNITS
1.	Key in the program		<input type="text"/>	<input type="text"/>	
2.	Store the following values		<input type="text"/>	<input type="text"/>	
	Greenwich Hour Angle of object (negative if east)	GHA,D.d	STO	1	
	Declination of object (negative if south)	DEC,D.d	STO	2	
	Semi-diameter of object (negative if U.L.)	SD,D.d	STO	3	
	Latitude (negative if south)	L,D.d	STO	4	
	Longitude (negative if east)	λ ,D.d	STO	5	
	Dip of the horizon	Dip,D.d	STO	6	
	Course	C,D.d	STO	7	
	Speed (in knots divided by 60)	S,D.d	STO	8	
	Time	t,H.h.	STO	9	
	Rate of change of GHA*	gha,D.d/hr	STO	1	
	Rate of change of dec*	dec.D.d/hr	STO	2	
3.	Enter a new time and compute new DR	t_{new} , H.MS	GSB	1	L,D.MS
			$x \leftrightarrow y$		λ ,D.MS
4.	Enter sextant altitude and compute intercept and azimuth	h_s , D.MS	<input type="text"/>	<input type="text"/>	
			GSB	2	a,mi.
			$x \leftrightarrow y$		Zn,D.d
5.	Update DR to MPP after GSB 2 in Step 4		GSB	7	a,D.d
	(i.e.: An in y; a in x)		GSB	3	L,D.MS
			$x \leftrightarrow y$		λ ,D.MS
*	Enter GHA or DEC for some time	Value ₁ ,D.MS	$\rightarrow H$		Value ₁ ,D.d
	Enter GHA or DEC for one hour earlier	Value ₂ ,D.MS	$\rightarrow H$		Value ₂ ,D.d
	OR		-		Rate D.d/hr
	Enter GHA or DEC for some time	Value ₁ ,DM.M	GSB	7	Value ₁ ,D.d
	Enter GHA or DEC for one hour earlier	Value ₂ ,DM.M	GSB	7	Value ₂ ,D.d
			-		Rate D.d/hr

Program Listings

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01 *LBL1		50 ÷	
02 →H		51 -	
03 RCL9		52 RCL3	
04 X+Y		53 +	
05 ST09	Update	54 ST.3	
06 X+Y	Time	55 RCL0	
07 -		56 RCL2	
08 ST.4		57 COS	
09 RC.1		58 →R	
10 x	Update	59 RCL4	
11 ST+1	GHA	60 ST.5	
12 RC.4	And	61 X+Y	
13 RC.2		62 →R	
14 x	DEC	63 ST.4	
15 ST+2		64 R↓	
16 RC.4		65 RC.5	
17 RCL8		66 RCL2	
18 x		67 SIN	
19 RCL7		68 →R	
20 X+Y		69 ST.5	
21 *LBL3		70 R↓	
22 →R	Update	71 RC.4	
23 ST+4	DR	72 +	
24 2		73 SIN ⁻¹	
25 ÷		74 ST.4	
26 RCL4		75 R↓	
27 X+Y		76 RC.5	
28 -		77 -	
29 COS		78 →P	
30 ÷		79 R↓	
31 ST-5		80 1	
32 RCL1		81 8	
33 RCL5		82 0	
34 -		83 +	
35 ST00		84 RC.3	
36 RCL5		85 RC.4	
37 →HMS	New λ	86 -	
38 RCL4		87 6	
39 →HMS		88 0	
40 RTN	New L	89 x	
41 *LBL2		90 RTN	
42 →H	Compute	91 *LBL7	
43 RCL6	a and Z _n	92 →HMS	
44 -		93 EEX	
45 ENT↑		94 2	
46 TAN		95 ÷	
47 1/X		96 →H	
48 6		97 RTN	
49 3			Convert DM.m to D.d

REGISTERS

0 LHA	1 GHA	2 DEC	3 SD	4 L	5 λ
6 Dip	7 C	8 S	9 t	10	11 gha
12 dec	13 H ₀	14 H _c	15 Used	16	17
18	19	20	21	22	23
24	25	26	27	28	29

SIGHT REDUCTION TABLE

This program calculates the computed altitude, H_c , and azimuth, Z_n , of a celestial body given the observer's latitude, L , and the local hour angle, LHA, and declination, d , of the body. It thus becomes a replacement for the nine volumes of HO 214. Moreover, the user need not bother with the distinctions of same name and contrary name; the program itself resolves all ambiguities of this type.

EQUATIONS:

$$H_c = \sin^{-1} [\sin d \sin L + \cos d \cos L \cos \text{LHA}]$$

$$Z_n = \begin{cases} Z; & \sin \text{LHA} < 0 \\ 360 - Z; & \sin \text{LHA} \geq 0 \end{cases}$$

$$Z = \cos^{-1} \left[\frac{\sin d - \sin L \sin H_c}{\cos L \cos H_c} \right]$$

REMARKS:

Southern latitudes and southern declinations must be entered as negative numbers.

The meridian angle t may be input in place of LHA, but if so, eastern meridian angles must be input as negative numbers.

The program assumes the calculator is set in DEG mode.

NOTE:

This program may also be used for star identification by entering observed azimuth in place of local hour angle and observed altitude in place of declination. The outputs are then declination and local hour angle instead of altitude and azimuth. The star may be identified by comparing this computed declination to the list of stars in The Nautical Almanac.

EXAMPLE 1:

Calculate the altitude and azimuth of the moon if its LHA is $2^\circ 39' 54''$ W and its declination $13^\circ 51' 06''$ S. The assumed latitude is $33^\circ 20' \text{N}$.

EXAMPLE 2:

Calculate the altitude and azimuth of REGULUS if its LHA is $36^\circ 39' 18''$ W and its declination is $12^\circ 12' 42''$ N. The assumed latitude is $33^\circ 30' \text{N}$.

EXAMPLE 3:

At 6:10 G.M.T. on January 12, 1977 a star peeked through the clouds over Corvallis ($L 44^\circ 34' \text{N}$, $123^\circ 17' \text{W}$). An alert observer using a bubble sextant quickly determined its altitude to be 26° and its azimuth 158° . Using the Nautical Almanac identify the star.

SOLUTIONS:

- | | | |
|-----|---------------|---------------|
| (1) | 33.20 ENT↑ | |
| | -13.5106 ENT↑ | |
| | 2.3954 GSB1 | |
| | 42.4447 *** | (Hc,D,MS) |
| | R/S | |
| | 183.5 *** | (Zn,dec.deg.) |
| (2) | 33.3000 ENT↑ | |
| | 12.1242 ENT↑ | |
| | 36.3918 GSB1 | |
| | 50.2425 *** | (Hc,D,MS) |
| | R/S | |
| | 246.3 *** | (Zn,dec.deg.) |

(3)

44.3400 ENT↑
26.0000 ENT↑
158.0000 GSB1
-16.3725 *** (d,D.MS)
R/S
339.4 *** (LHA,dec.deg.)
123.17 →H
+
462.7 *** (GHA,dec.deg.)
203.4 -
→HMS
259.2 *** (SHA,D.MS)

Program Listings

45

01 *LBL1		48 R↓	
02 →H	L	49 3	
03 ST02		50 6	
04 R↓		51 0	
05 →H		52 X→Y	
06 ST01	d	53 -	** Zn
07 R↓		54 RTN	
08 →H		55 *LBL0	
09 ST00	LHA	56 R↓	** Zn
10 SIN		57 RTN	
11 RCL1		58 R/S	
12 SIN			
13 X			
14 RCL0			
15 COS			
16 RCL1			
17 COS			
18 X			
19 RCL2			
20 COS			
21 X			
22 +			
23 ST03			
24 SIN→	Hc,dec.deg.		
25 ST04			
26 →HMS	Hc,D.MS		
27 FIX4	***		
28 R/S		** "PRINTX" may be inserted before "RTN".	
29 FIX1		*** "PRINTX" may be used to replace "R/S".	
30 RCL1			
31 SIN			
32 RCL3			
33 RCL0			
34 SIN			
35 X			
36 -			
37 RCL0			
38 COS			
39 ÷			
40 RCL4			
41 COS			
42 ÷			
43 COS→			
44 RCL2			
45 SIN	Z		
46 X<0?			
47 ST00			

REGISTERS					
0 L	1 d	2 LHA	3 Sin Hc	4 Hc	5
6	7	8	9	.0	.1
.2	.3	.4	.5	16	17
18	19	20	21	22	23
24	25	26	27	28	29

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