

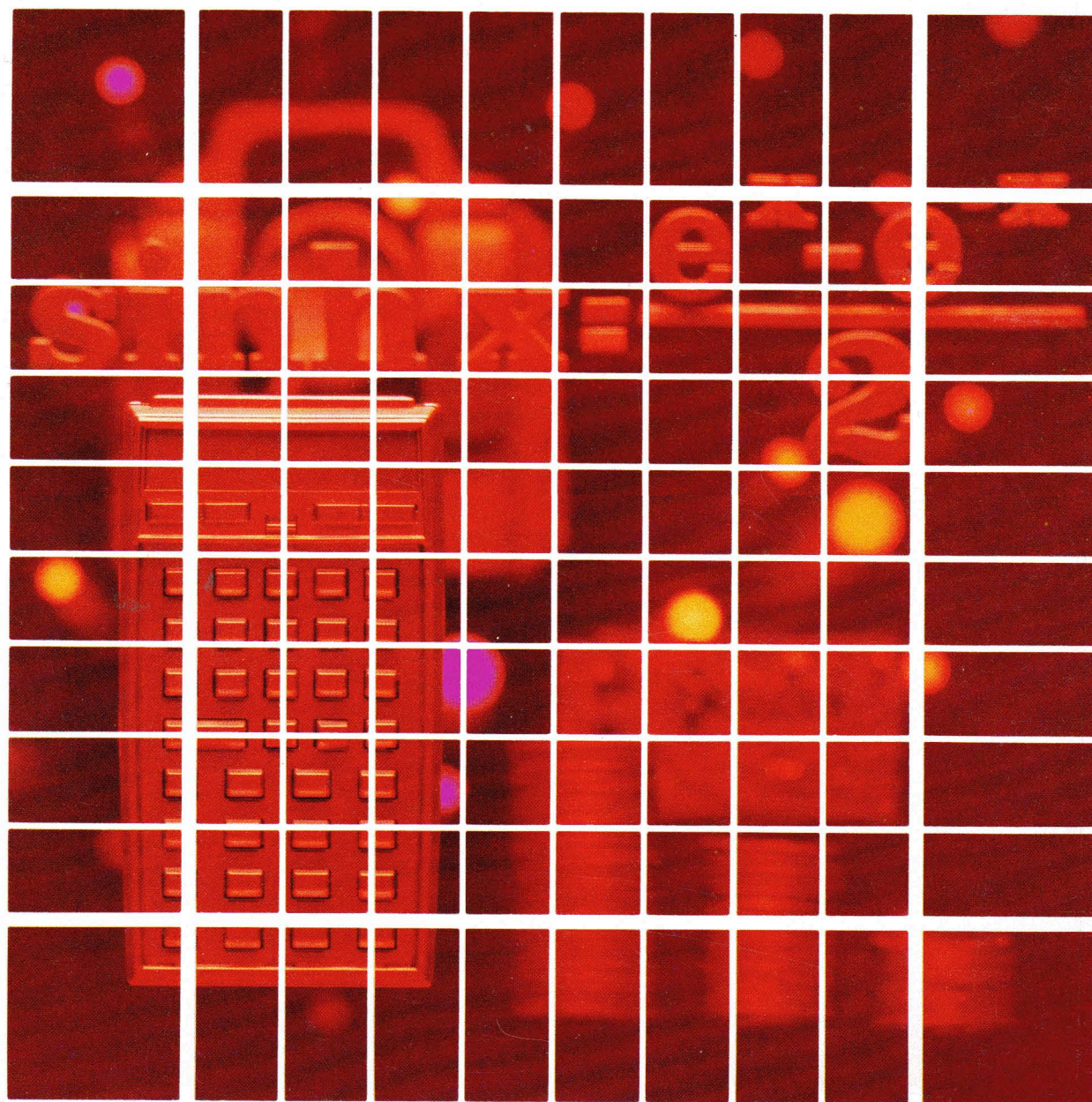
HEWLETT-PACKARD

HP-41

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Heating/Ventilating/ Air Conditioning

Includes barcode for easy software entry.



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INTRODUCTION

This HP-41C Solutions book was written to help you get the most from your calculator. The programs were chosen to provide useful calculations for many of the common problems encountered.

They will provide you with immediate capabilities in your everyday calculations and you will find them useful as guides to programming techniques for writing your own customized software. The comments on each program listing describe the approach used to reach the solution and help you follow the programmer's logic as you become and expert on your HP calculator.

KEYING A PROGRAM INTO THE HP-41C

There are several things that you should keep in mind while you are keying in programs from the program listings provided in this book. The output from the HP 82143A printer provides a convenient way of listing and an easily understood method of keying in programs without showing every keystroke. This type of output is what appears in this handbook. Once you understand the procedure for keying programs in from the printed listings, you will find this method simple and fast. Here is the procedure:

- At the end of each program listing is a listing of status information required to properly execute that program. Included is the SIZE allocation required. Before you begin keying in the program, press **XEQ** **ALPHA** **SIZE** **ALPHA** and specify the allocation (three digits; e.g., 10 should be specified as 010).

Also included in the status information is the display format and status of flags important to the program. To ensure proper execution, check to see that the display status of the HP-41C is set as specified and check to see that all applicable flags are set or clear as specified.

- Set the HP-41C to PRGM mode (press the **PRGM** key) and press **■** **GTO** **□** **□** to prepare the calculator for the new program.
- Begin keying in the program. Following is a list of hints that will help you when you key in your programs from the program listings in this handbook.
 - When you see " (quote marks) around a character or group of characters in the program listing, those characters are ALPHA. To key them in, simply press **ALPHA**, key in the characters, then press **ALPHA** again. So "SAMPLE" would be keyed in as **ALPHA** "SAMPLE" **ALPHA**.
 - The diamond in front of each LBL instruction is only a visual aid to help you locate labels in the program listings. When you key in a program, ignore the diamond.
 - The printer indication of divide sign is /. When you see / in the program listing, press **÷**.
 - The printer indication of the multiply sign is *. When you see * in the program listing, press **×**.
 - The † character in the program listing is an indication of the **APPEND** function. When you see †, press **■** **APPEND** in ALPHA mode (press **■** and the K key).
 - All operations requiring register addresses accept those addresses in these forms:

nn (a two-digit number)

IND nn (INDIRECT: **■**, followed by a two-digit number)

X, Y, Z, T, or L (a STACK address: **□** followed by X, Y, Z, T, or L)

IND X, Y, Z, T or L (INDIRECT stack: **■** **□** followed by X, Y, Z, T, or L)

Indirect addresses are specified by pressing **■** and then the indirect address. Stack addresses are specified by pressing **□** followed by X, Y, Z, T, or L. Indirect stack addresses are specified by pressing **■** **□** and X, Y, Z, T, or L.

Printer Listing	Keystrokes	Display
01♦LBL "SAMPLE"	■ LBL ALPHA SAMPLE ALPHA	01 LBL ^T SAMPLE
02 "THIS IS A"	ALPHA THIS IS A ALPHA	02 ^T THIS IS A
03 "†SAMPLE"	ALPHA ■ APPEND SAMPLE	03 ^T † SAMPLE
04 AVIEW	■ AVIEW ALPHA	04 AVIEW
05 6	6	05 6
06 ENTER↑	ENTER ↑	06 ENTER ↗
07 -2	2 CHS	07 -2
08 /	÷	08 /
09 ABS	XEQ ALPHA ABS ALPHA	09 ABS
10 STO IND	STO ■ □ L	10 STO IND L
11 "R3="	ALPHA R3= ■ ARCL 03	11 ^T R3=
12 ARCL 03	■ AVIEW	12 ARCL 03
13 AVIEW	ALPHA	13 AVIEW
14 RTN	■ RTN	14 RTN

TABLE OF CONTENTS

1.	OVERALL HEAT TRANSFER COEFFICIENT	1
	Sums convective and conductive coefficients to obtain the overall heat transfer coefficient.	
2.	INSULATION BREAK EVEN ANALYSIS	7
	Given economic and engineering parameters, computes the years to break even on an insulation investment.	
* 3.	AIR FLOW IN CIRCULAR DUCTS	13
	Can be used to analyze existing ducts or size new ducts.	
4.	AIR DUCT CONVERSION	24
	Converts from round ducts to equivalent rectangular ducts or from rectangular ducts to equivalent round ducts.	
* 5.	EQUATIONS OF STATE	31
	Relates pressure, temperature, volume, and amount of a gas using either the ideal gas law or the Redlich-Kwong model of real gas behavior.	
6.	BLACK BODY THERMAL RADIATION	41
	Computes thermal radiation as a function of temperature and wavelength for black bodies.	
** 7.	PSYCHROMETRIC PROPERTIES	50
	Computes properties of moist air based on temperature, pressure and either wet bulb temperature, relative humidity, or vapor pressure.	
* 8.	HEAT EXCHANGERS	63
	Correlates heat transfer for counterflow, parallel flow, parallel-counterflow and crossflow heat exchangers.	
9.	DECIBEL ADDITION AND SUBTRACTION	85
	Adds and subtracts sound levels in decibels.	
10.	TEMPERATURE CONVERSIONS	90
	Converts interchangeably between Kelvin, Fahrenheit, Celsius, and Rankin.	

* These programs require one memory module.

** This program requires two memory modules.

OVERALL HEAT TRANSFER COEFFICIENTS

This program sums convective and conductive coefficients to obtain the overall heat transfer coefficient for walls.

Equations:

$$U = \frac{1}{R_0 + R_1 + R_2 + \dots + R_n + \frac{1}{h_0} + \frac{1}{h_1} + \frac{1}{h_2} + \dots + \frac{1}{h_n} + \frac{x}{k_0} + \frac{x}{k_1} + \frac{x}{k_2} + \dots + \frac{x}{k_n} + \frac{1}{C_0} + \frac{1}{C_1} + \frac{1}{C_2} + \dots + \frac{1}{C_n}}$$

where:

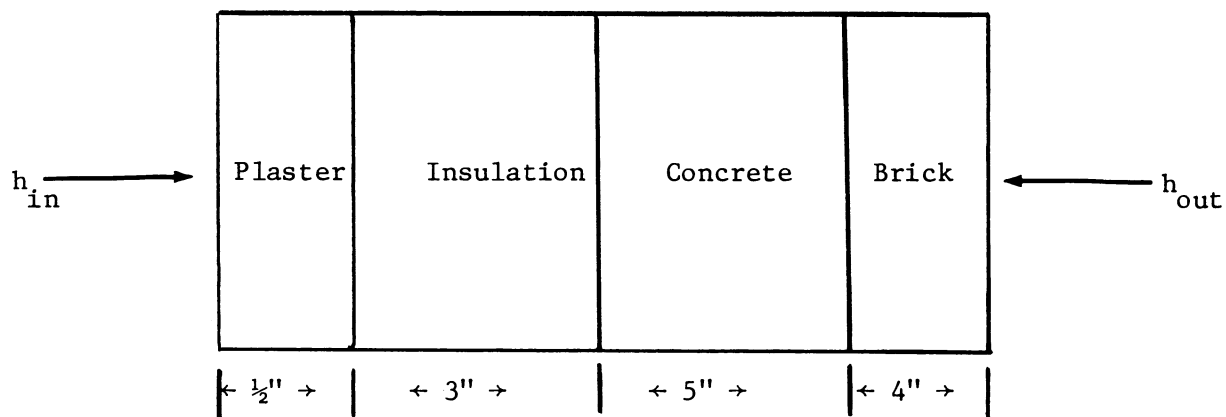
- Q is the heat transfer
- U is the overall heat transfer coefficient
- ΔT is the temperature difference across the wall
- R is the thermal resistance of a layer in the wall
- h is the convective resistance at a surface of the wall
- x is the thickness of a conductive layer
- k is the thermal conductivity of a substance
- C is the thermal conductance of a layer

Reference:

Threlkeld, James L.; Thermal Environmental Engineering; Prentice-Hall, Inc. 1970

Example:

What is the overall heat transfer coefficient for the wall below? What is the heat transfer for a 20°F temperature difference?



Layer	Coefficient	Symbol	Units
Inside Air	1.46	h	B/(hr) (ft ²) (°F)
Plaster	5	k	B/(hr) (ft ²) (°F/in)
Insulation	11	R	(hr) (ft ²) (°F)/BTU
Concrete	12	h	BTU/(hr) (ft ²) (°F/in)
Brick	36	C	BTU/(hr) (ft ²) (°F)
Outside Air	6	h	BTU/(hr) (ft ²) (°F)

Keystrokes:

[///] [FIX] 4
 [XEQ] [ALPHA] HEAT [ALPHA]
 1.46 [A]
 .5 [ENTER ↑] 5 [B]
 11 [D]
 5 [ENTER ↑] 12 [B]
 36 [C]
 6 [A]
 [R/S]
 20 [x]

Display:

H X↑K C R CL
 H X↑K C R CL
 H X↑K C R CL
 H X↑K C R CL
 H X↑K C R CL
 H X↑K C R CL
 H X↑K C R CL

U=0.0807

1.6134 (Btu/(ft²)(hr))

[illegible]

Program Listings

01*LBL "HEA T"		51	
02*LBL E	Initialize		
03 ADV	program.		
04 SF 27			
05 CLST			
06*LBL 01			
07 "H X↑K C	Define keyboard.		
R CL"			
08 PROMPT			
09 ADV		60	
10 "U="	Output U.		
11 ARCL X			
12 SF 21			
13 AVIEW			
14 GTO 01			
15*LBL A			
16 "H"			
17 XEQ 00	Add convective		
18 1/X	coefficient.		
19 GTO 02		70	
20*LBL B			
21 "X="	Add conductive		
22 ARCL Y	coefficient.		
23 FS? 55			
24 PRA			
25 "K"			
26 XEQ 00			
27 /			
28 GTO 02			
29*LBL C		80	
30 "C"	Add conductance.		
31 XEQ 00			
32 1/X			
33 GTO 02			
34*LBL D			
35 "R"	Add resistance.		
36 XEQ 00			
37*LBL 02			
38 RCL Y			
39 X≠0?		90	
40 1/X			
41 +			
42 1/X			
43 GTO 01	Print input.		
44*LBL 00			
45 "F="			
46 ARCL X			
47 FS? 55			
48 PRA			
49 RTN		00	

REGISTERS, STATUS, FLAGS, ASSIGNMENTS

DATA REGISTERS				STATUS			
00		50		SIZE <u>ANY</u> TOT. REG. <u>15</u> USER MODE			
				ENG _____ FIX _____ SCI _____ ON <u>X</u> OFF _____			
				DEG _____ RAD _____ GRAD _____			
05		55		FLAGS			
				#	INIT S/C	SET INDICATES	CLEAR INDICATES
10		60					
15		65					
20		70					
25		75					
30		80					
35		85					
				ASSIGNMENTS			
				FUNCTION	KEY	FUNCTION	KEY
40		90					
45		95					

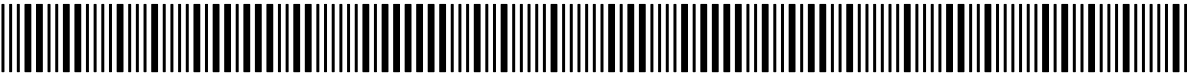
Overall Heat Transfer Coefficients

Registers: 16

ROW 1 (1 : 4)



ROW 2 (5 : 7)



ROW 3 (7 : 14)



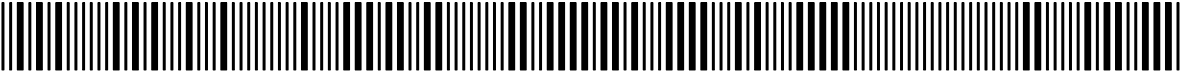
ROW 4 (14 : 20)



ROW 5 (21 : 26)



ROW 6 (26 : 33)



ROW 7 (33 : 40)



ROW 8 (41 : 48)



ROW 9 (48 - 50)



INSULATION BREAK EVEN ANALYSIS

This program calculates the number of years necessary for insulation to pay for itself based on heating costs. Inflation and the cost of money are accounted for.

Equations:

$$\text{YEARS} = \frac{-\ln \left(1 - \frac{\$/\text{FT}^2 (\% \text{INT} - \% \text{INF})}{\text{Yearly Savings}} \right)}{\ln \left(1 + \frac{\% \text{INT} - \% \text{INF}}{1 + \% \text{INF}} \right)}$$

$$\text{YEARLY SAVINGS} = \left(U - \frac{1}{(1/U + R)} \right) (\text{DEGDY}) (24) (\$/\text{BTU})$$

where:

YEARS is the number of years before insulation pays for itself.

$\$/\text{FT}^2$ is the cost of the insulation on a square foot basis.

%INT is the current lending rate to obtain insulation.

%INF is the expected inflation rate for the heat source being considered.

U is the overall heat transfer coefficient for the surface being considered with no insulation installed, $\text{Btu}/(\text{hr})(\text{ft}^2)(^\circ\text{F})$.

R is the thermal resistance of the insulating material, $(\text{hr})(\text{ft}^2)(^\circ\text{F})/\text{BTU}$.

DEGDY is the number of degree days for the area being considered.

See the ASHRAE GUIDE AND DATA BOOK for degree day information.

$\$/\text{BTU}$ is the current cost of heat per Btu.

Example:

A home in Seattle, Washington, (5145 degree days per year) is to have walls insulated with either R11 or R19 insulation costing 0.25 or 0.40 dollars per square foot respectively. The heat transfer coefficient for the uninsulated walls is $0.28 \text{ Btu}/(\text{hr})(\text{ft}^2)(^\circ\text{F})$. Natural gas at a cost of $3.66 \times 10^{-6} \text{ \$/Btu}$ is the heat source. Financing is available at 11% and energy is expected to inflate at 15% per year. How many years will it take for the two insulation choices to pay for themselves?

Keystrokes: (SIZE ≥ 009)

Display:

[////] [FIX] 2

[XEQ] [ALPHA] INSUL [ALPHA]

.28 [R/S]

3.66 [EEX] [CHS] 6 [R/S]

11 [R/S]

15 [R/S]

5145 [R/S]

11 [R/S]

.25 [R/S]

[R/S]*

19 [R/S]

.4 [R/S]

[R/S]*

U=?

\$/BTU=?

% INT=?

% INF=?

DEGDY=?

R=?

\$/FT2=?

YEARS=2.81

R=?

\$/FT2

YEARS=3.95

R=?

*Press [R/S] if you are not using a printer.

Program Listings

<pre> 01♦LBL "INS UL" 02 ADV 03 0 04 STO 00 05 "U" 06 XEQ "IN" 07 "\$/BTU" 08 XEQ "IN" 09 "%INT" 10 XEQ "IN" 11 "%INF" 12 XEQ "IN" 13 "DEGDY" 14 XEQ "IN" 15♦LBL 01 16 5 17 STO 00 18 "R" 19 XEQ "IN" 20 "\$/FT2" 21 XEQ "IN" 22 RCL 01 23 RCL 01 24 1/X 25 RCL 06 26 + 27 1/X 28 - 29 RCL 05 30 * 31 RCL 02 32 * 33 24 34 * 35 RCL 03 36 RCL 04 37 - 38 X=0? 39 GTO 00 40 100 41 / 42 STO 08 43 / 44 RCL 07 45 X<>Y 46 / 47 CHS 48 LN1+X 49 CHS </pre>	Input values.	<pre> 50 RCL 08 51 RCL 04 52 100 53 / 54 1 55 + 56 / 57 LN1+X 58 / 59♦LBL 03 60 ADV 61 "YEARS" 62 XEQ "0" 63 ADV 64 GTO 01 65♦LBL 00 66 RDN 67 RCL 07 68 RCL 04 69 % 70 + 71 X<>Y 72 / 73 GTO 03 74♦LBL "IN" 75 CF 22 76 1 77 ST+ 00 78 RCL IND 00 79 "t=" 80 ASTO Y 81 "t?" 82 CF 21 83 AVIEW 84 SF 21 85 CLA 86 ARCL Y 87 STOP 88 STO IND 00 89 FS? 22 90 FC? 55 91 RTN 92 ARCL X 93 PRA 94 RTN 95♦LBL "0" 96 "t=" 97 ARCL X 98 AVIEW </pre>	
	Calculate savings.		Output years.
	Calculate years.		Special case where inflation equals interest.
			Input subroutine.
			Output subroutine.

REGISTERS, STATUS, FLAGS, ASSIGNMENTS

DATA REGISTERS				STATUS			
00	DATA PRINTER	50		SIZE 009	TOT. REG. 37	USER MODE	
	U			ENG	FIX	SCI	ON OFF
	\$ /BTU			DEG	RAD	GRAD	
	%INT						
	%INF						
05	DEGDY	55		FLAGS			
	R			#	INIT S/C	SET INDICATES	CLEAR INDICATES
	\$ /FT2						
	(%INT-%INF) /100						
10		60					
15		65					
20		70					
25		75					
30		80					
35		85					
				ASSIGNMENTS			
				FUNCTION	KEY	FUNCTION	KEY
40		90					
45		95					

ROW 1 (1 : 5)



ROW 2 (5 : 8)



ROW 3 (8 : 11)



ROW 4 (11 : 13)



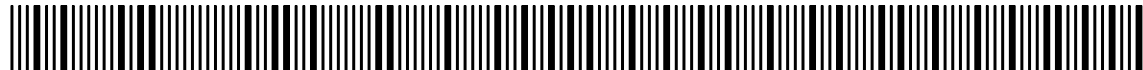
ROW 5 (14 : 19)



ROW 6 (20 : 24)



ROW 7 (25 : 36)



ROW 8 (37 : 46)



ROW 9 (47 : 57)



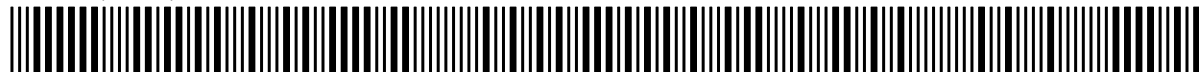
ROW 10 (58 : 63)



ROW 11 (64 : 74)



ROW 12 (74 : 79)



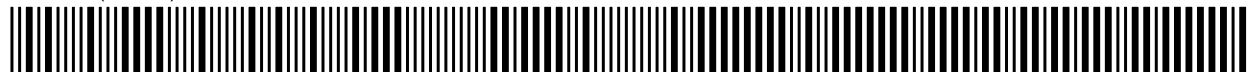
ROW 13 (79 : 85)



ROW 14 (86 : 93)



ROW 15 (93 : 98)



ROW 16 (99 - 99)



AIR FLOW IN CIRCULAR DUCTS

(Requires one memory module)

This program can be used to compute the pressure difference, velocity or volumetric flow rate for air in circular, metal, HVAC ducts.

Equations:

$$v^2 = \frac{dP/\rho}{2 \left(f \frac{L}{D} + \frac{K_T}{4} \right)}$$

For laminar flow ($Re < 2300$)

$$f = 16/Re$$

For turbulent flow ($Re > 2300$)

$$\frac{1}{\sqrt{f}} = 1.737 \ln \frac{D}{\epsilon} + 2.28 - 1.737 \ln \left(4.67 \frac{D}{\epsilon Re \sqrt{f}} + 1 \right)$$

is solved by Newton's method.

$$\frac{1}{\sqrt{f}_0} = 1.737 \ln \frac{D}{\epsilon} + 2.28$$

is used as an initial guess in the iteration.

$$\mu = 1.101 \times 10^{-6} (T)^{1.5} / (T+200) \text{ (N}\cdot\text{s/m}^2\text{)}$$

$$\rho = 1.201 \left(\frac{P}{29.92} \right) \left(\frac{530}{T} \right) \text{ (kg/m}^3\text{)}$$

where:

Re is the Reynolds number, defined as $\rho Dv/\mu$;

D is the pipe diameter;

ϵ is the dimension of irregularities in the conduit surface

f is the Fanning friction factor for conduit flow;

dP is the pressure difference along the conduit;

ρ is the density of the fluid;

μ is the viscosity of the fluid;

L is the conduit length;

- v is the average fluid velocity;
 K_T is the total of the applicable fitting coefficients in table 1;
 T is the air temperature in degrees Rankine.
 P is the air pressure in inches of mercury.

Table 1
Fitting Coefficients

Fitting	K
90° elbow	0.4-0.9
Standard 45° elbow	0.35-0.42
Tee, through side outlet	1.5
Tee, straight through	.4
180° bend	1.6
Entrance to circular pipe	0.25-0.50
Sudden expansion	$(1 - A_{up}/A_{dn})^2*$
Acceleration from $v = 0$ to $v = V_{entrance}$	1.0

Remarks:

For rectangular ducts, use the duct conversion program of this solution book.

This program assumes incompressible flow, thus accuracy will degenerate as velocity increases above 12,000 feet per minute.

No algorithm gives reliable outputs for transition flow ($2300 < Re < 4000$). If this condition is encountered, the program will halt displaying "TRANSITION". You may press [R/S] and the program will continue to an answer but the answer may have little or no relation to reality.

References:

Welty, Wicks, Wilson; *Fundamentals of Momentum, Heat and Mass Transfer*, John Wiley and Sons, Inc., 1969.

Baumeister, *Mark's Standard Handbook For Mechanical Engineers*, Seventh Edition, McGraw-Hill, 1967, p. 12-136.

* A_{up} is the upstream area and A_{dn} is the downstream area.

Example 1:

What pressure drop will force 6000 cubic feet per minute of 70°F air through 100 feet of 20 inch straight conduit. The atmospheric pressure is 29 inches of mercury.

Keystrokes:	(SIZE $\geq$ 018)	Display:
[///]	[FIX] 2	
[XEQ]	[ALPHA] AIRDUCT [ALPHA]	T,F=?
70	[R/S]	INH20=?
29	[R/S]	L,FT=?
100	[R/S]	ΣK=?
0	[R/S]	D,IN=?
20	[R/S]	SELECT KEY: dP V Q
[C]		Q,CFM=?
6000	[R/S]	INH20=0.41
[R/S]*		V,FPM=2750.73
[R/S]*		D,IN=?

* Press [R/S] if you are not using a printer.

Example 2:

The flow rate in Example 1 is to be increased to 15,000 cubic feet per minute by increasing the conduit diameter. What diameter is necessary?

Keystrokes:	Display:
First run Example 1. You should have the "D,IN=?" prompt in the Display. Guess a diameter of 30 inches.	

30	[R/S]	SELECT KEY: dP V Q
[A]		INH20=?
[R/S]		V,FPM=3,551.69
[R/S]*		Q,CFM=17,430.93
[R/S]*		D,IN=?

The 30 inch duct will be adequate but try a 28 inch duct.

28	[R/S]	SELECT KEY: dP V Q
[A]		INH20=?
[R/S]		V,FPM=3,401.48
[R/S]*		Q,CFM=14,542.07
[R/S]*		D,IN=?

Since duct is available only in even size use 30 inch duct.

User Instructions

				SIZE: 018
STEP	INSTRUCTIONS	INPUT	FUNCTION	DISPLAY
1.	Load program			
2.	Initialize program		[XEQ] AIRDUCT	T,F=?
3.	Key in air temperature in degrees			
	Fahrenheit.	T	[R/S]	INHG=?
4.	Key in average atmospheric pressure in			
	inches of mercury.	P _{atm}	[R/S]	L,FT=?
5.	Key in length of duct in feet	L	[R/S]	ΣK
6.	Key in sum of fitting coefficients from			
	Table 1.	ΣK	[R/S]	D,IN=?
7.	Key in duct diameter in inches	D	[R/S]	SELECT KEY:
				dP V Q
8.	If you know pressure difference, press			
	[A]		[A]	INH20=?
	If you know velocity, press [B]		[B]	V,FPM=?
	If you know volumetric flow rate press			
	[C]		[C]	Q, CFM=?
9.	Key in known selected in step 8 and			
	calculate remaining unknowns.	known	[R/S]	UNKNOWN ₁
			[R/S]*	UNKNOWN ₂
			[R/S]*	D,IN=?
10.	For a new diameter, or step 8 input, go to			
	step 7. For a new case go to step 2. In			
	either case, key in only values which			
	change.			
*	Press [R/S] if you are not using a printer.			

Program Listings

01♦LBL "AIR DUCT" 02 ADV 03 0 04 STO 00 05 "T,F" 06 XEQ "IN" 07 "INHG" 08 XEQ "IN" 09 RCL 01 10 460 11 + 12 STO 10 13 RCL X 14 1.5 15 Y↑X 16 1.101 E- 6 17 * 18 RCL Y 19 200 20 + 21 / 22 STO 16 23 RCL 02 24 29.92 25 / 26 530 27 RCL 10 28 / 29 * 30 1.201 31 * 32 STO 17 33 762 E-7 34 STO 03 35 3 36 STO 00 37 "L,FT" 38 .3048 39 ST/ 04 40 XEQ "IN" 41 .3048 42 ST* 04 43 1 44 ST+ 00 45 "ΣK" 46 XEQ "IN" 47♦LBL 15 48 4 49 STO 00	Calculate and store viscosity, density and surface irregularities.	50 "D,IN" 51 .0254 52 ST/ 05 53 XEQ "IN" 54 .0254 55 ST* 05 56 SF 27 57 "SELECT KEY:" 58 CF 21 59 AVIEW 60 SF 21 61 PSE 62♦LBL 01 63 "dP V Q" 64 PROMPT 65 GTO 01 66♦LBL A 67 6 68 STO 00 69 248.8 70 ST/ 07 71 "INH20" 72 XEQ "IN" 73 248.8 74 ST* 07 75 SF 03 76 XEQ 09 77♦LBL 03 78 RND 79 STO 15 80 XEQ 08 81 RND 82 RCL 15 83 X<>Y 84 X*Y? 85 GTO 03 86 XEQ "Re" 87 "V,FPM" 88 RCL 08 89 196.9 90 * 91 GTO 00 92♦LBL C 93 7 94 STO 00 95 "Q,CFM" 96 XEQ 11 97 * 98 * 99 STO 08	Input D.
---	--	---	--

Program Listings

100 XEQ "IN"		151 STO 07	
101 XEQ 11		152 RTN	
102 *		153♦LBL 09	
103 /		154 ADV	
104 STO 08		155 RCL 16	
105 XEQ 10		156 RCL 17	
106 XEQ "Re"	Calculate	157 /	Guess $1/\sqrt{f}$.
107 "INH20"	pressure drop.	158 STO 09	
108 RCL 07		159 RCL 05	
109 248.8		160 RCL 03	
110 /		161 /	
111 XEQ "O"		162 STO 10	
112 "V,FPM"		163 LN	
113 RCL 08		164 1.737	
114 196.9		165 STO 11	
115 *		166 *	
116 XEQ "O"		167 2.28	
117 ADV		168 +	
118 GTO 15		169 STO 12	
119♦LBL B	Input velocity.	170 STO 13	
120 7		171 FS? 03	
121 STO 00		172 GTO 07	
122 "V,FPM"		173♦LBL 08	Special case
123 5.08 E-3		174 16	for low velocity
124 ST/ 08		175 RCL 08	flow.
125 XEQ "IN"		176 RCL 05	
126 5.08 E-3		177 *	
127 ST* 08		178 RCL 09	
128 XEQ 10	Calculate	179 /	
129 XEQ "Re"	pressure drop.	180 STO 14	
130 "INH20"		181 2300	
131 RCL 07	Output routine.	182 X<=Y?	
132 248.8		183 GTO 02	
133 /		184 RDN	
134♦LBL 00		185 /	
135 XEQ "O"		186 SQRT	
136 "Q,CFM"		187 1/X	
137 XEQ 11		188 STO 13	
138 *		189 GTO 07	
139 *		190♦LBL 02	
140 XEQ "O"		191 RCL 12	
141 ADV		192 RCL 13	
142 GTO 15		193 -	
143♦LBL 10		194 4.67	
144 CF 03	Calculate	195 RCL 10	
145 XEQ 09	pressure drop.	196 *	
146 RCL 08		197 RCL 14	
147 X↑2		198 /	
148 *		199 RCL 13	
149 RCL 17		200 *	
150 *		201 1	Turbulent flow friction factor.

Program Listings

202 +		252 2300	
203 STO 00		253 RCL 14	
204 LN		254 X<=Y?	
205 RCL 11		255 RTN	
206 *		256 4000	
207 -		257 X>Y?	
208 RCL 00		258 PROMPT	
209 1/X		259 RTN	
210 CHS		260♦LBL 11	
211 1		261 RCL 08	
212 +		262 RCL 05	
213 RCL 11		263 X↑2	
214 *		264 PI	
215 RCL 13		265 *	
216 /		266 4	
217 1		267 /	
218 +		268 2119	
219 /		269 RTN	
220 ST+ 13		270♦LBL "IN"	
221 RCL 13		271 CF 22	
222 /		272 1	
223 ABS		273 ST+ 00	
224 1 E-3		274 RCL IND	
225 X<=Y?		00	
226 GTO 02		275 "I="	
227♦LBL 07	Compute velocity.	276 ASTO Y	
228 RCL 13		277 "I?"	
229 1/X		278 CF 21	
230 X↑2		279 AVIEW	
231 RCL 04		280 SF 21	
232 *		281 CLA	
233 RCL 05		282 ARCL Y	
234 /		283 STOP	
235 RCL 06		284 STO IND	
236 4		00	
237 /		285 FS? 22	
238 +		286 FC? 55	
239 ST+ X		287 RTN	
240 RCL 07		288 ARCL X	
241 RCL 17		289 PRA	
242 /		290 RTN	
243 X<>Y		291♦LBL "O"	
244 FC? 03		292 "I="	
245 RTN		293 ARCL X	
246 /		294 AVIEW	
247 SQRT			
248 STO 08			
249 RTN			
250♦LBL "Re"			
251 "TRANSIT			
ION"			
	Check for transition.	00	

Convert between velocity and volumetric flow rate.

Input routine.

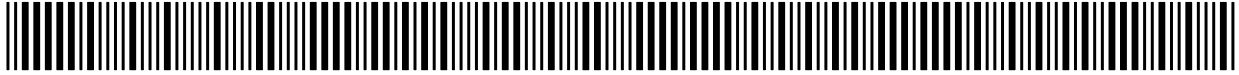
Output routine.

[illegible]

ROW 1 (1 : 3)



ROW 2 (4 : 7)



ROW 3 (7 : 13)



ROW 4 (14 : 17)



ROW 5 (18 : 24)



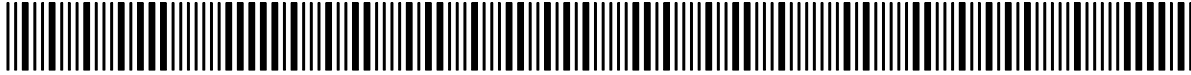
ROW 6 (24 : 30)



ROW 7 (30 : 36)



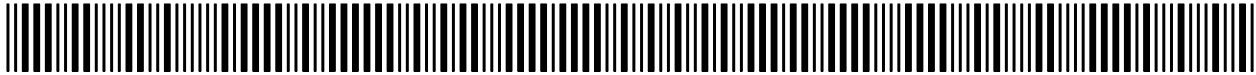
ROW 8 (37 : 40)



ROW 9 (40 : 44)



ROW 10 (45 : 50)



ROW 11 (50 : 53)



ROW 12 (53 : 57)



ROW 13 (57 : 60)



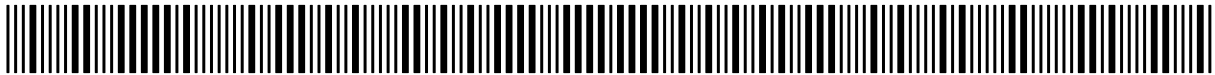
ROW 14 (60 : 65)



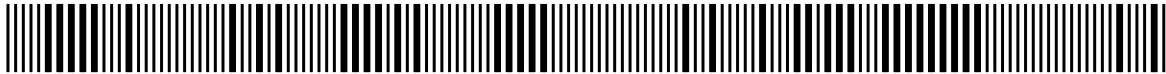
ROW 15 (66 : 71)



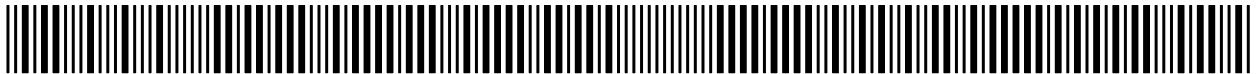
ROW 16 (71 : 73)



ROW 17 (74 : 80)



ROW 18 (81 : 87)

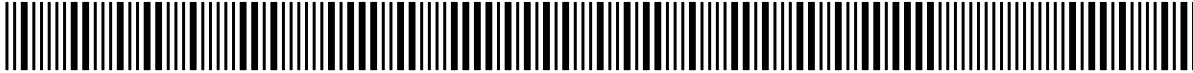


Air Flow in Circular Ducts

ROW 19 (87 : 92)



ROW 20 (92 : 97)



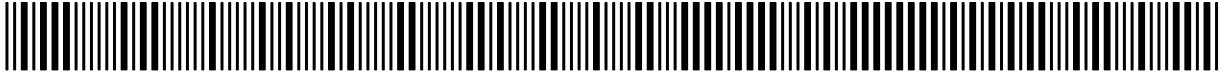
ROW 21 (98 : 105)



ROW 22 (105 : 108)



ROW 23 (109 : 112)



ROW 24 (112 : 117)



ROW 25 (118 : 122)



ROW 26 (123 : 125)



ROW 27 (126 : 129)



ROW 28 (129 : 132)



ROW 29 (132 : 136)



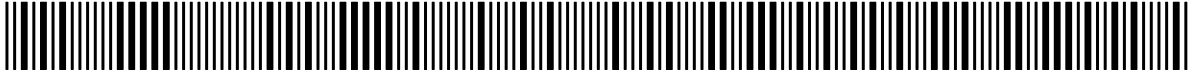
ROW 30 (137 : 143)



ROW 31 (144 : 152)



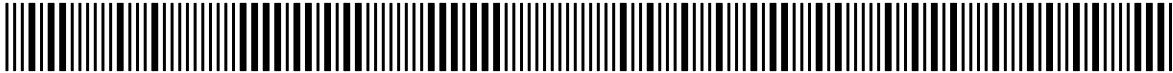
ROW 32 (153 : 163)



ROW 33 (164 : 169)



ROW 34 (170 : 179)



ROW 35 (180 : 188)



ROW 36 (189 : 197)

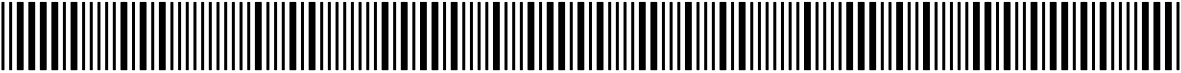


Air Flow in Circular Ducts

ROW 37 (198 : 210)



ROW 38 (211 : 222)



ROW 39 (223 : 231)



ROW 40 (232 : 242)



ROW 41 (243 : 250)



ROW 42 (250 : 252)



ROW 43 (252 : 259)



ROW 44 (260 : 269)



ROW 45 (270 : 274)



ROW 46 (275 : 280)



ROW 47 (281 : 288)



ROW 48 (289 : 293)



ROW 49 (294 - 295)



AIR DUCT CONVERSION

This program converts a round, metal, HVAC, air duct to an equivalent rectangular air duct. The inverse conversion is also provided.

Equations:

$$D = \frac{1.3 (ab)^{0.625}}{(a + b)^{0.25}}$$

where:

- a is the depth (or width) of a rectangular duct in inches.
- b is the width (or depth) of a rectangular duct in inches.
- D is the approximate diameter for an equivalent round duct.

Reference:

Wolfe, James M.; Air Duct Conversion; HP-67/97 Users' Library Program 03046D.
Baumeister, Mark's Standard Handbook for Mechanical Engineers, Seventh Edition,
McGraw Hill, 1967, p. 12-137

Example 1:

A duct measuring 15 inches by 8 inches is to be replaced with a round duct.
What diameter duct is required?

Keystrokes: (SIZE ≥ 003)	Display:
[////] [FIX] 2	
[XEQ] [ALPHA] REC-RND [ALPHA]	a=?
15 [R/S]	b=?
8 [R/S]	D=12.00
[R/S]*	a=?

Example 2:

A duct sizing program computes a diameter of 30 inches for a duct. Clearances only allow 24 inches in the vertical direction. What horizontal dimension is necessary for a rectangular duct?

Keystrokes: (SIZE $\geq$ 003)

Display:

[////] [FIX] 2

[XEQ] [ALPHA] RND-REC [ALPHA]

D=?

30 [R/S]

a=?

24 [R/S]

b=32

[R/S]*

D=?

*Press [R/S] if you are not using a printer.

				SIZE: 003
STEP	INSTRUCTIONS	INPUT	FUNCTION	DISPLAY
1.	Load program.			
2.	For circular to rectangular conversions,			
	go to step 3b.			
3.	Initialize for rectangular to circular			
	conversion.		[XEQ] REC-RND	a=?
4.	Key in depth.	a	[R/S]	b=?
5.	Key in width and calculate diameter.	b	[R/S]	D=
			[R/S]*	a=?
6.	For a new case go to step 4a. Key in			
	only values which change. For the			
	inverse conversion, go to step 3b.			
3b.	Initialize for circular to rectangular			
	conversion		[XEQ] RND-REC	D=?
4b.	Key in diameter	D	[R/S]	a=?
5b.	Key in the depth or width and calculate			
	the other dimension	a	[R/S]	b=
			[R/S]*	D=?
6b.	For a new case, go to step 4b. Key in			
	only values which change. For the			
	inverse conversion, go to step 3.			
*	Press [R/S] if you are not using a printer.			

Program Listings

<pre> 01♦LBL "REC -RND" 02♦LBL 01 03 ADV 04 0 05 STO 00 06 "a" 07 XEQ "IN" 08 "b" 09 XEQ "IN" 10 ADV 11 RCL 01 12 * 13 .625 14 Y↑X 15 RCL 01 16 RCL 02 17 + 18 SQRT 19 SQRT 20 / 21 1.3 22 * 23 "D" 24 .5 25 + 26 INT 27 XEQ "0" 28 GTO 01 29♦LBL "RND -REC" </pre>	Input a and b.	<pre> 49 RCL 00 50 RCL 02 51 * 52 .625 53 Y↑X 54 1.3 55 * 56 RCL 00 57 RCL 02 58 + 59 SQRT 60 SQRT 61 RCL 01 62 * 63 - 64 RCL 00 65 -.375 66 Y↑X 67 RCL 02 68 .625 69 Y↑X 70 * 71 .8125 72 * 73 RCL 02 74 RCL 00 75 + 76 -.75 77 Y↑X 78 RCL 01 79 * 80 4 81 / 82 - 83 / 84 ST- 00 85 RCL 00 86 / 87 ABS 88 .25 89 X<=Y? 90 GTO 03 91 RCL 00 92 .5 93 + 94 INT 95 "b" 96 XEQ "0" 97 GTO 02 98♦LBL "IN" 99 CF 22 </pre>	Iterate by Newton's method to find b.
<pre> 30♦LBL 02 31 ADV 32 0 33 STO 00 34 "D" 35 XEQ "IN" 36 "a" 37 XEQ "IN" 38 RCL 02 39 RCL 01 40 * 41 RCL 02 42 ST+ X 43 RCL 01 44 - 45 / 46 STO 00 47 ADV 48♦LBL 03 </pre>		<pre> 61 RCL 01 62 * 63 - 64 RCL 00 65 -.375 66 Y↑X 67 RCL 02 68 .625 69 Y↑X 70 * 71 .8125 72 * 73 RCL 02 74 RCL 00 75 + 76 -.75 77 Y↑X 78 RCL 01 79 * 80 4 81 / 82 - 83 / 84 ST- 00 85 RCL 00 86 / 87 ABS 88 .25 89 X<=Y? 90 GTO 03 91 RCL 00 92 .5 93 + 94 INT 95 "b" 96 XEQ "0" 97 GTO 02 98♦LBL "IN" 99 CF 22 </pre>	
<pre> 41 RCL 02 42 ST+ X 43 RCL 01 44 - 45 / 46 STO 00 47 ADV 48♦LBL 03 </pre>	Guess b based on wetted perimeter.	<pre> 87 ABS 88 .25 89 X<=Y? 90 GTO 03 91 RCL 00 92 .5 93 + 94 INT 95 "b" 96 XEQ "0" 97 GTO 02 98♦LBL "IN" 99 CF 22 </pre>	Output b.
			Input subroutine.

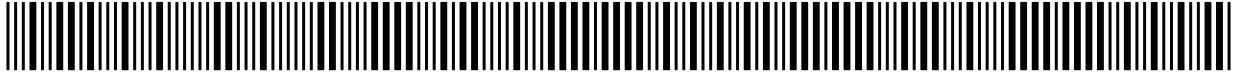
Program Listings

100 1		51	
101 ST+ 00			
102 RCL IND			
00			
103 "I="			
104 ASTO Y			
105 "I?"			
106 CF 21			
107 AVIEW			
108 SF 21		60	
109 CLA			
110 ARCL Y			
111 STOP			
112 STO IND			
00			
113 FS? 22			
114 FC? 55			
115 RTN			
116 ARCL X			
117 PRA		70	
118 RTN			
119 LBL "0"	Output subroutine		
120 "I="			
121 ARCL X			
122 AVIEW			
30		80	
40		90	
50		00	

ROW 1 (1 : 3)



ROW 2 (4 : 9)



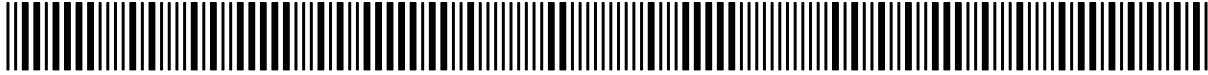
ROW 3 (9 : 18)



ROW 4 (19 : 27)



ROW 5 (27 : 29)



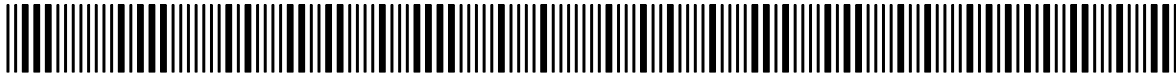
ROW 6 (29 : 36)



ROW 7 (36 : 44)



ROW 8 (45 : 54)



ROW 9 (54 : 65)



ROW 10 (65 : 71)



ROW 11 (71 : 77)



ROW 12 (78 : 88)



ROW 13 (88 : 96)



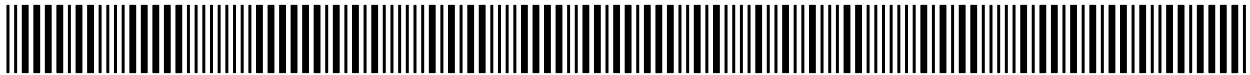
ROW 14 (96 : 101)



ROW 15 (101 : 106)



ROW 16 (107 : 114)



ROW 17 (115 : 120)



ROW 18 (120 - 123)



EQUATIONS OF STATE

(Requires one memory module)

This program provides both ideal gas and Redlich-Kwong equations of state. Given four of the five state variables, the fifth is calculated. For the Redlich-Kwong solution, the critical pressure and temperature of the gas must be known. They are not needed for ideal gas solutions.

Values of the Universal Gas Constants

Value of R	Units of R	Units of P	Units of V	Units of T
8.314	N-m/g mole-K	N/m ²	m ³ /g mole	K
83.14	cm ³ -bar/g mole-K	bar	cm ³ /g mole	K
82.05	cm ³ -atm/g mole-K	atm	cm ³ /g mole	K
0.7302	atm-ft ³ /lb mole-°R	atm	ft ³ /lb mole	°R
10.73	psi-ft ³ /lb mole-°R	psi	ft ³ /lb mole	°R
1545	psf-ft ³ /lb mole-°R	psf	ft ³ /lb mole	°R

Critical Temperatures and Pressures

Substance	T _c , K	T _c , °R	P _c , ATM
Ammonia	405.6	730.1	112.5
Argon	151	272	48.0
Carbon dioxide	304.2	547.6	72.9
Carbon monoxide	133	239	34.5
Chlorine	417	751	76.1
Helium	5.3	9.5	2.26
Hydrogen	33.3	59.9	12.8
Nitrogen	126.2	227.2	33.5
Oxygen	154.8	278.6	50.1
Water	647.3	1165.1	218.2
Dichlorodifluoromethane	384.7	692.5	39.6
Dichlorofluoromethane	451.7	813.1	51.0
Ethane	305.5	549.9	48.2
Ethanol	516.3	929.3	63
Methanol	513.2	923.8	78.5
n-Butane	425.2	765.4	37.5
n-Haxane	507.9	914.2	29.9
n-Pentane	469.5	845.1	33.3
n-Octane	568.6	1023.5	24.6
Trichlorofluoromethane	471.2	848.1	43.2

Equations:

Ideal gas: $PV = nRT$

Redlich-Kwong:
$$P = \frac{nRT}{(V - b)} - \frac{a}{T^{1/2} V (V + b)}$$

$$a = 4.934 b nRT_c^{1.5}$$

$$b = 0.0867 \frac{nRT_c}{P_c}$$

where:

P is the absolute pressure;

V is the volume;

n is the number of moles present;

R is the universal gas constant;

T is the absolute temperature;

T_c is the critical temperature;

P_c is the critical pressure.

Remarks:

P, V, n and T must have units compatible with R.

At low temperatures or high pressures, the ideal gas law does not represent the behavior of real gases.

No equation of state is valid for all substances or over an infinite range of conditions. The Redlich-Kwong equation gives moderate to good accuracy for a variety of substances over a wide range of conditions. Results should be used with caution and tempered by experience.

Solutions for V, n, R and T, using the Redlich-Kwong equation, require an iterative technique. Newton's method is employed using the ideal gas law to generate the initial guess. Iteration time is generally a function of the amount of deviation from ideal gas behavior. For extreme cases, the routine may fail to converge entirely, resulting in "DATA ERROR".

Example 1:

0.63 g moles of air are enclosed in a 25,000 cm³ space at 1200 K. What is the pressure in bars? Assume ideal gas behavior.

Keystrokes:

[XEQ] [ALPHA] SIZE [ALPHA] 015

[XEQ] [ALPHA] ID [ALPHA]

0 [R/S]

25000 [R/S]

0.63 [R/S]

83.14 [R/S]

1200 [R/S]

Display:

P?

V?

N?

R?

T?

P=2.51

Example 2:

The specific volume of a gas in a container is 800 cm³/g mole. The temperature will reach 400 K. What will the pressure be, according to the Redlich-Kwong relation?

$$P_c = 48.2 \text{ atm}$$

$$T_c = 305.5 \text{ K}$$

$$R = 82.05 \text{ cm}^3 - \text{atm/g mole-K}$$

Keystrokes:

[XEQ] [ALPHA] RK [ALPHA]

305.5 [R/S]

48.2 [R/S]

0 [R/S]

800 [R/S]

1 [R/S]

82.05 [R/S]

400 [R/S]

Display:

TC?

PC?

P?

V?

N?

R?

T?

P=36.29

[illegible]

Program Listings

01♦LBL "ID" 02 0 03 SF 00 04 GTO 00 05♦LBL "RK" 06 1 07 CF 00 08 "TC?" 09 PROMPT 10 STO 13 11 "PC?" 12 PROMPT 13 STO 14 14♦LBL 00 15 SF 02 16 CF 01 17 FIX 2 18 "P?" 19 PROMPT 20 5 21 XEQ 00 22 "V?" 23 PROMPT 24 6 25 XEQ 00 26 "N?" 27 PROMPT 28 7 29 XEQ 00 30 "R?" 31 PROMPT 32 8 33 XEQ 00 34 "T?" 35 PROMPT 36 CF 02 37 9 38♦LBL 00 39 CF 01 40 STO 01 41 RDN 42 STO IND 01 43 X≠0? 44 GTO 01 45 R↑ 46 STO 10 47 1 48 STO IND 01 49♦LBL 01	Initialization	50 FS? 02 51 RTN 52 GTO IND 10 53♦LBL 05 54 "P="	----- Calculate unknown
		55 GTO 00 56♦LBL 06 57 "V="	
		58♦LBL 00 59 RCL 07 60 RCL 08 61 * 62 RCL 09 63 * 64 RCL 05 65 RCL 06 66 * 67 / 68 STO IND 10 69 GTO 00 70♦LBL 07 71 SF 01 72 "N="	
		73 GTO 01 74♦LBL 08 75 SF 01 76 "R="	
		77 GTO 01 78♦LBL 09 79 "T="	
		80 SF 01 81♦LBL 01 82 RCL 05 83 RCL 06 84 * 85 RCL 07 86 / 87 RCL 08 88 / 89 RCL 09 90 / 91 STO IND 10 92♦LBL 00 93 FS? 00 94 GTO 10 95 XEQ 01 96 GTO 00 97♦LBL 02	

Program Listings

98 FS? 01	-----	145 *	
99 XEQ 01		146 X↑2	
100♦LBL 00	If ideal, display	147 /	
101 RCL 00		148 RCL 00	
102 RCL 09		149 RCL 09	
103 *	-----	150 *	
104 RCL 06	Calculate using	151 RCL 04	
105 RCL 12	Redlich-Kwong	152 X↑2	
106 -	equations	153 /	
107 STO 04		154 -	
108 /		155 RTN	
109 RCL 11		156♦LBL 09	$\frac{\partial P}{\partial T}$
110 RCL 09		157 RCL 00	
111 SQRT		158 RCL 04	
112 /		159 /	
113 STO 02		160 RCL 02	
114 RCL 06		161 2	
115 /		162 /	
116 LASTX		163 RCL 09	
117 RCL 12		164 /	
118 +		165 RCL 06	
119 STO 03		166 /	
120 /		167 RCL 03	
121 -		168 /	
122 RCL 05		169 +	
123 -		170 RTN	
124 XEQ IND		171♦LBL 07	
10		172♦LBL 08	$\frac{\partial P}{\partial n}$ or $\frac{\partial P}{\partial R}$
125 /		173 RCL 09	
126 ST- IND		174 RCL 06	
10		175 *	
127 RCL IND		176 RCL 04	
10		177 X↑2	
128 /		178 /	
129 ABS		179 RCL 06	
130 1 E-4		180 ENTER↑	
131 X<=Y?		181 +	
132 GTO 02		182 RCL 12	
133 RCL IND		183 +	
10		184 RCL 00	
134 GTO 10		185 /	
135♦LBL 06		186 RCL 06	
136 RCL 06		187 /	
137 ENTER↑		188 RCL 03	
138 +	$\frac{\partial P}{\partial V}$	189 X↑2	
139 RCL 12		190 /	
140 +		191 RCL 02	
141 RCL 02		192 *	
142 *		193 -	
143 RCL 03		194 RCL 00	
144 RCL 06		195 *	

Program Listings

196 RCL IND		51	
10			
197 /			
198 RTN			
199♦LBL 05			
200 LASTX			
201 +			
202 STO 05			
203 GTO 10			
204♦LBL 01	Calculate a, b	60	
205 RCL 07			
206 RCL 08			
207 *			
208 STO 00			
209 .0867			
210 RCL 14			
211 /			
212 X<>Y			
213 RCL 13			
214 *			
215 *		70	
216 STO 12			
217 LASTX			
218 *			
219 RCL 13			
220 SQRT			
221 *			
222 4.934			
223 *			
224 STO 11			
225 RTN		80	
226♦LBL 10	Display		
227 ARCL X			
228 AVIEW			
229 STOP			
230 .END.			
40		90	
50		00	

DATA REGISTERS				STATUS			
00	NR	50		SIZE	015	TOT. REG.	61
	temp storage index			ENG		FIX	2
	a/T ^{1/2}			DEG		RAD	
	(V + b)					GRAD	
	(V - b)						
05	P	55		FLAGS			
	V			#	INIT S/C	SET INDICATES	CLEAR INDICATES
	n			00		Ideal	Redlich-Kwong
	f			01		Calc a, b	
	T			02		Inputting data	Calculate
10	control	60					
	a						
	b						
	T _c						
	P _c						
15		65					
20		70					
25		75					
30		80					
35		85					
				ASSIGNMENTS			
				FUNCTION KEY		FUNCTION KEY	
40		90					
45		95					

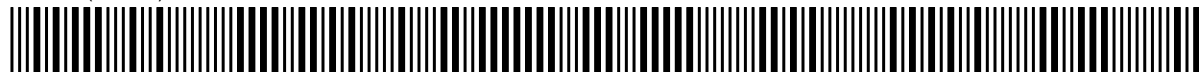
ROW 1 (1 : 5)



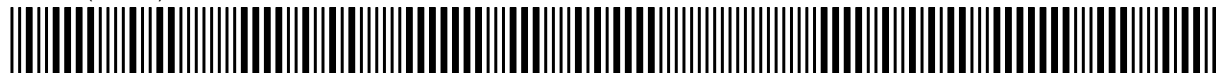
ROW 2 (5 : 10)



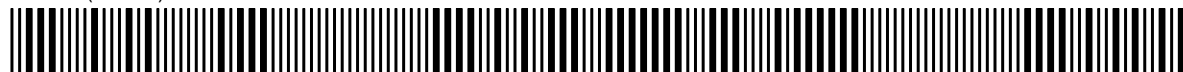
ROW 3 (11 : 17)



ROW 4 (18 : 24)



ROW 5 (25 : 30)



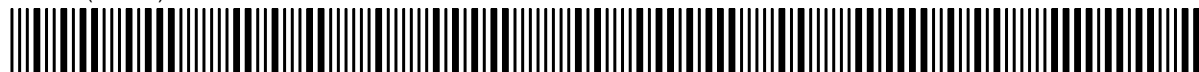
ROW 6 (30 : 37)



ROW 7 (38 : 47)



ROW 8 (48 : 55)



ROW 9 (55 : 65)



ROW 10 (66 : 73)



ROW 11 (73 : 79)



ROW 12 (80 : 91)



ROW 13 (91 : 98)



ROW 14 (98 : 108)



ROW 15 (109 : 121)



ROW 16 (122 : 130)



ROW 17 (130 : 138)



ROW 18 (139 : 151)



Equations of State

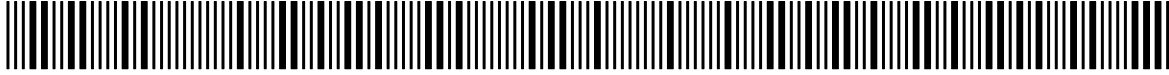
ROW 19 (152 : 164)



ROW 20 (165 : 177)



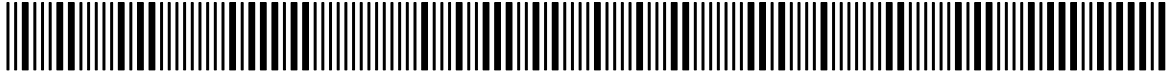
ROW 21 (178 : 190)



ROW 22 (191 : 202)



ROW 23 (203 : 210)



ROW 24 (211 : 222)



ROW 25 (222 : 230)



ROW 26 (230 - 230)



BLACK BODY THERMAL RADIATION

(Requires one memory module)

Bodies with finite temperatures emit thermal radiation. The higher the absolute temperature, the more thermal radiation emitted. Bodies which emit the maximum possible amount of energy at every wavelength for a specified temperature are said to be black bodies. While black bodies do not actually exist in nature, many surfaces may be assumed to be black for engineering considerations.

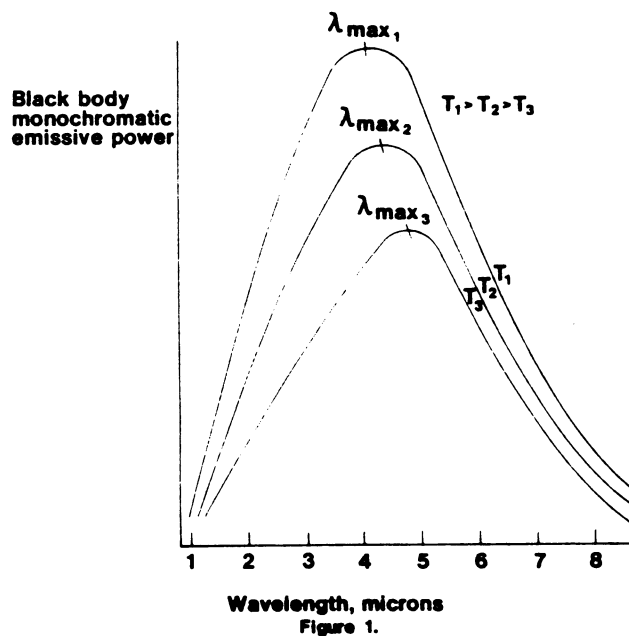


Figure 1.

Notes:

A half minute or more may be required to obtain $E_b(0-\lambda)$ or $E_b(\lambda_1-\lambda_2)$ since the integration is numerical.

Sources differ on values for constants. This could yield small discrepancies between published tables and program outputs.

Figure 1 is a representation of black body thermal emission as a function of wavelength. Note that as temperature increases, the area under the curves (total emissive power $E_b(0-\infty)$) increases. Also note that the wavelength of maximum emissive power λ_{max} shifts to the left as temperature increases.

This program calculates the wavelength of maximum emissive power for a given temperature, the temperature for which a given wavelength would be the wavelength of maximum emissive power, the total emissive power over all wavelengths, the emissive power at a particular wavelength, the emissive power from zero to a specified wavelength, and the emissive power between specified wavelengths.

Equations:

$$\lambda_{\max} T_{\lambda_{\max}} = c_3$$

$$E_{b(0-\infty)} = \sigma T^4$$

$$E_{b\lambda} = \frac{2\pi c_1}{\lambda^5 (e^{c_2/\lambda T} - 1)}$$

$$\begin{aligned} E_{b(0-\lambda)} &= \int_0^\lambda E_{b\lambda} d\lambda \\ &= 2\pi c_1 \sum_{k=1}^{\infty} -T/kc_2 e^{-\frac{kc_2}{T\lambda}} \left[\left(\frac{1}{\lambda} \right)^3 + \frac{3T}{\lambda^2 kc_2} \right. \\ &\quad \left. + \frac{6}{\lambda} \left(\frac{T}{kc_2} \right)^2 + 6 \left(\frac{T}{kc_2} \right)^3 \right] \end{aligned}$$

$$E_{b(\lambda_1 - \lambda_2)} = E_{b(0-\lambda_2)} - E_{b(0-\lambda_1)}$$

where:

$\lambda_{\max}$ is the wavelength of maximum emissivity in microns;

T is the absolute temperature in °R or K;

$E_{b(0-\infty)}$ is the total emissive power in Btu/hr-ft² or Watts/cm²;

$E_{b\lambda}$ is the emissive power at λ in Btu/hr-ft²-μm or Watts/cm²-μm;

$E_{b(0-\lambda)}$ is the emissive power for wavelengths less than λ in Btu/hr-ft² or Watts/cm²;

$E_{b(\lambda_1 - \lambda_2)}$ is the emissive power for wavelengths between λ_1 and λ_2 in Btu/hr-ft² or Watts/cm².

$$\begin{aligned} c_1 &= 1.8887982 \times 10^7 \text{ Btu-}\mu\text{m}^4/\text{hr-ft}^2 \\ &= 5.9544 \times 10^3 \text{ W}\mu\text{m}^4/\text{cm}^2 \end{aligned}$$

$$c_2 = 2.58984 \times 10^4 \mu\text{m-}^\circ\text{R} = 1.4388 \times 10^4 \mu\text{m-K}$$

$$c_3 = 5.216 \times 10^3 \mu\text{m-}^\circ\text{R} = 2.8978 \times 10^3 \mu\text{m-K}$$

$$\sigma = 1.713 \times 10^{-9} \text{ Btu/hr-ft}^2 \cdot ^\circ\text{R}^4 = 5.6693 \times 10^{-12} \text{ W/cm}^2 \cdot \text{K}^4$$

$$\sigma_{\text{exp}} = 1.731 \times 10^{-9} \text{ Btu/hr-ft}^2 \cdot ^\circ\text{R}^4 = 5.729 \times 10^{-12} \text{ W/cm}^2 \cdot \text{K}^4$$

References: HP-67/97 Users' Library Program.

Example:

What percentage of the radiant output of a lamp is in the visible range (0.4 to 0.7 microns) if the filament of the lamp is assumed to be a black body at 2400K?

Keystrokes: (SIZE $\geq$ 009)

Display:

[USER]

(set USER mode)

[XEQ] [ALPHA] BB [ALPHA]

UNITS?

SI [R/S]

TEMP?

2400 [R/S]

WAVELENGTH?

.4 [R/S]

SOLVE

[F]

WV LNTH 2?

.7 [R/S]

EbL-L=4.9679

[C]

EbTOT=188.0938

[$\div$]

0.0264

100 [x]

2.6412

[illegible]

Program Listings

01*LBL "BB"	Initialize and prompt for units	47 RCL 06	Calculate $T(\lambda_{\max})$
02 CLRG		48 /	
03 CF 22		49 "TEMP="	
04 "UNITS?"		50 ARCL X	
05 AON		51 PROMPT	
06 PROMPT		52*LBL C	Calculate E_b total
07 AOFF		53 RCL 05	
08 ASTO X		54 X↑2	
09 GTO IND		55 X↑2	
X		56 RCL 04	
10*LBL "SI"	Store units	57 *	
11 5954.4		58 "EbTOT="	
12 STO 01		59 ARCL X	
13 14388		60 PROMPT	
14 STO 02		61*LBL D	Calculate $E_{b\lambda}$
15 2897.8		62 RCL 01	
16 STO 03		63 ENTER↑	
17 5.6693 E		64 +	
-12		65 PI	
18 STO 04		66 *	
19 GTO 00		67 RCL 06	
20*LBL "EN"		68 5	
21 18887982		69 Y↑X	
22 STO 01		70 /	
23 25998.4		71 RCL 02	
24 STO 02		72 RCL 06	
25 5216		73 /	
26 STO 03		74 RCL 05	
27 .171312		75 /	
E-08		76 E↑X	
28 STO 04		77 1	
29*LBL 00	Input prompting	78 -	
30 "TEMP?"		79 /	
31 PROMPT		80 "EbL="	
32 STO 05		81 ARCL X	
33 "WAVELEN		82 PROMPT	
GTH?"		83*LBL E	Calculate $E_b(0-\lambda)$
34 PROMPT		84 0	
35 STO 06		85 STO 08	
36 "SOLVE"		86 STO 07	
37 PROMPT		87*LBL 01	
38*LBL A	Calculate $\lambda_{\max}$	88 RDN	
39 RCL 03		89 CLX	
40 RCL 05		90 RCL 08	
41 /		91 RCL 02	
42 "WL MAX="		92 RCL 05	
"		93 /	
43 ARCL X		94 -	
44 PROMPT		95 STO 08	
45*LBL B		96 3	
46 RCL 03		97 X<>Y	

Program Listings

98 /		149 "WV LNTH	
99 RCL 06		2?"	
100 X↑2		150 PROMPT	
101 /		151 ENTER↑	
102 LASTX		152 ENTER↑	
103 1/X		153 SF 00	
104 RCL 06		154 XEQ E	
105 /		155 X<>Y	
106 -		156 RCL 06	
107 6		157 STO 00	
108 RCL 06		158 RDN	
109 /		159 STO 06	
110 RCL 08		160 SF 00	
111 X↑2		161 XEQ E	
112 /		162 -	
113 -		163 ABS	
114 6		164 RCL 00	
115 RCL 08		165 STO 06	
116 X↑2		166 RDN	
117 /		167 "EbL-L="	
118 RCL 08		168 ARCL X	
119 /		169 PROMPT	
120 +		170 .END.	
121 RCL 08			
122 RCL 06			
123 /			
124 E↑X			
125 *			
126 RCL 08			
127 /			
128 ST+ 07	80		
129 RCL 07			
130 /			
131 1 E-05			
132 X<=Y?			
133 GTO 01			
134 RDN			
135 CLX			
136 RCL 07			
137 ENTER↑			
138 +	90		
139 PI			
140 *			
141 RCL 01			
142 *			
143 FS?C 00			
144 RTN			
145 "Eb0-L="			
146 ARCL X.			
147 PROMPT			
148*LBL F	Calculate		
	$E_b(\lambda_1-\lambda_2)$	00	

DATA REGISTERS				STATUS			
00	λ	50		SIZE <u>009</u> TOT. REG. <u>57</u> USER MODE			
	C ₁			ENG _____ FIX <u>4</u> SCI _____ ON <u>X</u> OFF _____			
	C ₂			DEG _____ RAD _____ GRAD _____			
	C ₃						
	σ						
05	T	55		FLAGS			
	λ, λ'			#	INIT S/C	SET INDICATES	CLEAR INDICATES
	sum			00		Used	
	kc ₂ /T			22		Used	
10		60					
15		65					
20		70					
25		75					
30		80					
35		85					
				ASSIGNMENTS			
				FUNCTION		KEY	FUNCTION
40		90					KEY
45		95					

ROW 1 (1 : 4)



ROW 2 (4 : 10)



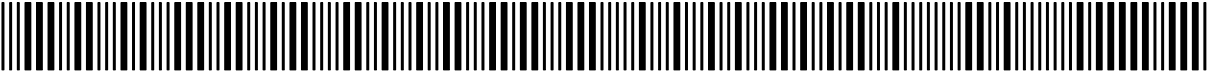
ROW 3 (10 : 13)



ROW 4 (13 : 17)



ROW 5 (17 : 20)



ROW 6 (20 : 23)



ROW 7 (23 : 27)



ROW 8 (27 : 30)



ROW 9 (30 : 33)



ROW 10 (33 : 36)



ROW 11 (36 : 42)



ROW 12 (42 : 49)



ROW 13 (49 : 57)



ROW 14 (58 : 62)



ROW 15 (63 : 75)



ROW 16 (76 : 83)



ROW 17 (83 : 95)



ROW 18 (96 : 108)



Black Body Thermal Radiation

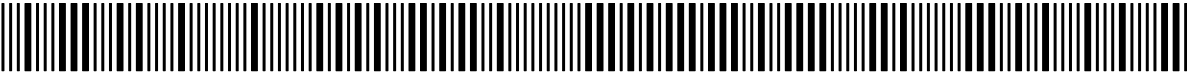
ROW 19 (109 : 121)



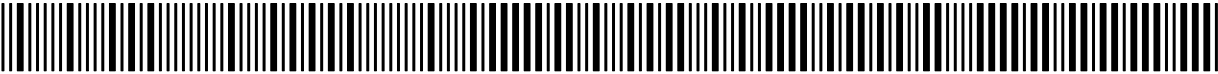
ROW 20 (122 : 131)



ROW 21 (131 : 141)



ROW 22 (142 : 146)



ROW 23 (147 : 149)



ROW 24 (149 : 158)



ROW 25 (159 : 167)



ROW 26 (167 - 170)



PSYCHROMETRIC PROPERTIES

(Requires two memory modules)

Given pressure, drybulb temperature and either wet bulb temperature or relative humidity or vapor pressure, this program computes wet bulb temperature, dew point temperature, vapor pressure, humidity ratio, relative humidity, enthalpy and specific volume.

Either English or SI units may be used in problem solution.

Variable	English Units	SI Units
Temperature	°F	°C
Pressure	psi	kPa
Humidity Ratio	lb _m /lb _m dry air	kg/kg dry air
Relative Humidity	%	%
Enthalpy	Btu/lb _m dry air	kJ/kg dry air
Specific Volume	ft ³ /lb _m dry air	dm ³ /kg dry air

Temperatures may range from -40°F (-40°C) to 300 °F (150°C). For temperatures less than the ice point, vapor is assumed in equilibrium with ice.

Total pressure may range from 1.0 psi (7.0 kPa) to 50.0 psi (345.0 kPa).

Relative humidity may range between 0.0 and 100%.

Specific humidity must be less than 0.2.

If limits are exceeded program will halt with alpha diagnostic in Display.

Equations:

$$W = \frac{c_{p,a}(t_{wb} - t_{db}) + \omega_{sat,wb}(h_{g,wb} - h_{f,wb})}{h_{v,db} - h_{f,wb}}$$

$$c_{p,a} = 0.240 \text{ Btu/lb}_m^{\circ}\text{F} = 1.0048 \text{ kJ/kg}^{\circ}\text{C}$$

$$h_v = h_g = a + bt$$

$$a = 1061.0 \text{ Btu/lb}_m = 2501.0 \text{ kJ/kg}$$

$$b = 0.445 \text{ Btu/lb}_m^{\circ}\text{F} = 1.8631 \text{ kJ/kg}^{\circ}\text{C}$$

IF $t \geq 32^{\circ}\text{F}$ or 0°C

THEN $h_f = (t - c)d$

$$c = 32^{\circ}\text{F} = 0^{\circ}\text{C}$$

$$d = 1 \text{ Btu/lb}_m^{\circ}\text{F} = 4.1868 \text{ kJ/kg}^{\circ}\text{C}$$

IF $t < 32^{\circ}\text{F}$ or 0°C

THEN $h_f = h_i = [(t-c)0.467 + e]d$
 $e = -143.956^{\circ}\text{F} = -79.97556^{\circ}\text{C}$

$$H = c_{p,a} t_{db} + W h_{v,db}$$

$$W = \frac{R_{air}}{R_{vapor}} = \frac{PV}{P - PV} = \frac{R_{air}}{R_{vapor}} = 0.622$$

(also used to calculate P_{vapor})

$$P_{sat} = f e^{g/(t+h)}$$

t = temperature, $^{\circ}\text{F}$ or $^{\circ}\text{C}$

$$e = 2.718282$$

IF $t \geq 32^{\circ}\text{F}$ or 0°C

THEN $f = 2.04466 \cdot 10^6 \text{ psi} = 1.40974 \cdot 10^7 \text{ kPa}$
 $g = -7071.3^{\circ}\text{F} = -3928.5^{\circ}\text{C}$
 $h = 385^{\circ}\text{F} = 231.667^{\circ}\text{C}$

IF $t < 32^{\circ}\text{F}$ or 0°C

THEN $f = 5.24506 \cdot 10^8 \text{ psi} = 3.61633 \cdot 10^9 \text{ kPa}$
 $g = -11071^{\circ}\text{F} = -6150.6^{\circ}\text{C}$
 $h = 460^{\circ}\text{F} = 273.33^{\circ}\text{C}$

$$V = \frac{R_{air} T}{P_{total} - P_{vapor}}$$

$$REL = P_{vapor}/P_{sat,db}$$

where:

P is the total pressure.

PV is the vapor pressure

t_{db} is the dry bulb temperature.

P_{sat} is the saturation pressure.

t_{wb} is the wet bulb temperature.

t_{dp} is the dew point temperature.

W is the humidity ratio.

REL is the relative humidity.

h is the enthalpy.

V is the specific volume.

Reference:

HP-67 Users' Library Program 867D, Psychrometric Properties, Donald H. Madsen.

Example 1:

$P = 101.325 \text{ kPa}$, $T_{wb} = 20^\circ\text{C}$ $T_{db} = 25^\circ$

Keystrokes: (SIZE $\geq$ 010)

Display:

[////] [FIX] 4

[XEQ] [ALPHA] PSYCHSI [ALPHA]

P=?

101.325 [R/S]

Tdb=?

25 [R/S]

PSAT=3.1762

[R/S]*

SELECT KEY: TWb REL PV

[A]

TWb=?

20 [R/S]

TdP=17.6023

[R/S]*

PV=2.0166

[R/S]*

W=0.0126

[R/S]*

REL=63.4931

[R/S]*

H=57.2983

[R/S]*

V=860.7494

[R/S]*

P=?

*Press [R/S] if you are not using a printer.

Example 2:

$P = 25 \text{ psi}$, $Tdb = 70.0^\circ\text{F}$, $PV = 0.182 \text{ psi}$

Keystrokes:

Display:

[////] [FIX] 4

[XEQ] [ALPHA] PSYCHE [ALPHA]

P=?

25 [R/S]

Tdb=?

70 [R/S]

PSAT=0.3640

[R/S]*

SELECT KEY: TWb REL PV

[E]

PV=?

.182 [R/S]

TWb=60.8398

[R/S]*

TdP=50.5726

[R/S]*

PV=0.1820

[R/S]*

W=0.0046

[R/S]*

REL=49.9988

[R/S]*

H=21.7817

[R/S]*

V=7.8987

[R/S]*

P=?

*Press [R/S] if you are not using a printer.

User Instructions

				SIZE: 010
STEP	INSTRUCTIONS	INPUT	FUNCTION	DISPLAY
1.	Load program			
2.	Initialize program for English units, or		[XEQ] PSYCHE	
	SI units.		[XEQ] PSYCHSI	P=?
3.	Key in total pressure.	P	[R/S]	Tdb=?
4.	Key in dry bulb temperature.	Tdb	[R/S]	PSAT=
			[R/S]*	SELECT KEY:
				TWb REL PV
5.	Press [A] if you know wet bulb temperature,		[A]	TWb=?
	[C] if you know relative humidity, or [E]		[B]	REL=?
	if you know vapor pressure, then go to		[C]	PV=?
	6a, 6b, or 6c.			
6a.	Key in wet bulb temperature and start			
	calculation.	TWb	[R/S]	
6b.	Key in relative humidity and start			
	calculation.	REL	[R/S]	TWb=
6c.	Key in vapor pressure and start calculation	PV	[R/S]	TWb=
7.	See outputs of:			
	Dew Point temperature,		[R/S]*	TdP=
	Vapor Pressure,		[R/S]*	PV=
	Humidity Ratio,		[R/S]*	W=
	Relative Humidity,		[R/S]*	REL=
	Enthalpy,		[R/S]*	H=
	Specific Volume		[R/S]*	V=
			[R/S]*	P=?
8.	For a new case using the same units, go to			
	step 3. Key in only values which change.			
*	Press [R/S] if you are not using a printer			

Program Listings

<pre> 01♦LBL "PSY CHSI" 02 SF 00 03 GTO 00 04♦LBL "PSY CHE" 05 CF 00 06♦LBL 00 07 0 08 STO 00 09 ADV 10 "P" 11 XEQ "IN" 12 "Tdb" 13 XEQ "IN" 14 XEQ F 15 ADV 16 "PSAT" 17 XEQ "0" 18 STO 06 19 ADV 20 "SELECT KEY:" 21 CF 21 22 AVIEW 23 SF 21 24 PSE 25♦LBL 22 26 SF 27 27 "TWb RE L PV" 28 PROMPT 29 GTO 22 30♦LBL A 31 2 32 STO 00 33 "TWb" 34 XEQ "IN" 35 XEQ F 36 XEQ 03 37 "TWb HIG H" 38 X<0? 39 PROMPT 40 XEQ 04 41 "TWb LOW " 42 X<0? 43 PROMPT 44 STO 07 45 .2 </pre>	Initialize for SI units. Initialize for English units. Input T and T_{db}. Calculate P_{sat}. Prompt user to select key [A], [C], or [E]. Input T_{wb}.	<pre> 46 "SPC HUM >=.2" 47 X<=Y? 48 PROMPT 49 RDN 50 RCL 01 51 * 52 RCL 07 53 .622 54 + 55 / 56 "TWb>Tdb " 57 XEQ 05 58 ADV 59 GTO 18 60♦LBL C 61 3 62 STO 00 63 "REL" 64 XEQ "IN" 65 ADV 66 RCL 02 67 STO 03 68 XEQ F 69 X<>Y 70 % 71 STO 08 72 GTO 00 73♦LBL E 74 RCL 02 75 STO 03 76 7 77 STO 00 78 "PV" 79 XEQ "IN" 80 "VP>Tdb" 81 ADV 82 XEQ 05 83 RCL 08 84♦LBL 00 85 XEQ 03 86 "VP>P" 87 X<0? 88 PROMPT 89 STO 07 90 .2 91 "W>.2" 92 X<=Y? 93 PROMPT 94 FS? 00 </pre>	Input relative humidity. Input vapor pressure.
---	---	--	--

Program Listings

```

95 80
96 FC? 00
97 140
98 STO 09
99 CF 02
100♦LBL 01
101 RCL 09
102 FS?C 02
103 CHS
104 ST- 03
105 2
106 ST/ 09
107 RCL 03
108 XEQ F
109 XEQ 03
110 X<0?
111 GTO 01
112 XEQ 04
113 RCL 07
114 -
115 X<0?
116 SF 02
117 ABS
118 1 E-5
119 X<=Y?
120 GTO 01
121 GTO 08
122♦LBL 06
123 FC? 00
124 .445
125 FS? 00
126 1.8631
127 *
128 FC? 00
129 1061
130 FS? 00
131 2501
132 +
133 X<>Y
134 32
135 FS? 00
136 CLX
137 -
138 X<0?
139 XEQ 07
140 FC? 00
141 1
142 FS? 00
143 4.1868
144 *
145 -

```

Calculate T_{wb} .

Calculate
enthalpy
difference.

```

146 RTN
147♦LBL 07
148 .467
149 *
150 FC? 00
151 -143.956
152 FS? 00
153 -79.9755
6
154 +
155 RTN
156♦LBL 05
157 STO 08
158 RCL 06
159 /
160 1
161 X<>Y
162 X>Y?
163 PROMPT
164 1 E2
165 *
166 STO 04
167 RTN
168♦LBL 08
169 RCL 03
170 "TWb"
171 XEQ "0"
172♦LBL 18
173 RCL 08
174 X=0?
175 GTO 09
176 32
177 FS? 00
178 CLX
179 XEQ F
180 X>Y?
181 GTO 00
182 RCL 08
183 FS? 00
184 1.40974
E7
185 FC? 00
186 2.04466
E6
187 /
188 LN
189 1/X
190 FS? 00
191 -3928.5
192 FC? 00
193 -7071.3

```

Relative
humidity
calculation.

Print results.

Program Listings

```

194 *
195 FS? 00
196 231.667
197 FC? 00
198 385
199 -
200 GT0 11
201*LBL 00
202 RCL 08
203 FS? 00
204 3.61633
E9
205 FC? 00
206 5.24506
E8
207 /
208 LN
209 1/X
210 FS? 00
211 -6150.6
212 FC? 00
213 -11071
214 *
215 FS? 00
216 273.33
217 FC? 00
218 460
219 -
220 GT0 11
221*LBL F
222 32
223 FS? 00
224 CLX
225 X>Y?
226 GT0 00
227 RDN
228 FS? 00
229 231.667
230 FC? 00
231 385
232 +
233 FS? 00
234 -3928.5
235 FC? 00
236 -7071.3
237 X<>Y
238 /
239 E↑X
240 FS? 00
241 1.40974
E7
242 FC? 00

```

Saturation
pressure
subroutine.

```

243 2.04466
E6
244 *
245 RTN
246*LBL 00
247 RDN
248 FS? 00
249 273.33
250 FC? 00
251 460
252 +
253 FS? 00
254 -6150.6
255 FC? 00
256 -11071
257 X<>Y
258 /
259 E↑X
260 FS? 00
261 3.61633
E9
262 FC? 00
263 5.24506
E8
264 *
265 RTN
266*LBL 03
267 "WSAT OR
  VP=P"
268 .622
269 X<>Y
270 *
271 RCL 01
272 LASTX
273 -
274 X=0?
275 PROMPT
276 /
277 RTN
278*LBL 04
279 RCL 03
280 RCL 03
281 XEQ 06
282 *
283 RCL 03
284 RCL 02
285 -
286 FC? 00
287 .24
288 FS? 00
289 1.0048

```

Saturation
pressure for
sub-icepoint
conditions.

Calculate
specific
humidity from
vapor pressure.

Calculate
specific
humidity from
wet and dry
bulb temperatures.

Program Listings

290 *		341 "V"	
291 +		342 XEQ "0"	
292 RCL 03		343 GTO 00	
293 RCL 02		344♦LBL "IN"	
294 XEQ 06		345 CF 22	Input subroutine.
295 /		346 1	
296 RTN		347 ST+ 00	
297♦LBL 11		348 RCL IND	
298 "TdP"	Output values.	00	
299 XEQ "0"		349 "I="	
300♦LBL 09		350 ASTO Y	
301 RCL 08		351 "I?"	
302 "PV"		352 CF 21	
303 XEQ "0"		353 AVIEW	
304 RCL 07		354 SF 21	
305 "W"		355 CLA	
306 XEQ "0"		356 ARCL Y	
307 RCL 04		357 STOP	
308 "REL"		358 STO IND	
309 XEQ "0"		00	
310 RCL 02		359 FS? 22	
311 FC? 00		360 FC? 55	
312 .24		361 RTN	
313 FS? 00		362 ARCL X	
314 1.0048		363 PRA	
315 *		364 RTN	
316 32		365♦LBL "0"	Output subroutine
317 FS? 00		366 "I="	
318 ST- X		367 ARCL X	
319 RCL 02		368 AVIEW	
320 XEQ 06			
321 RCL 07			
322 *			
323 +			
324 "H"			
325 XEQ "0"			
326 RCL 02			
327 FC? 00			
328 459.67			
329 FS? 00			
330 273.15			
331 +			
332 FC? 00			
333 .3701			
334 FS? 00			
335 286.7			
336 *			
337 RCL 01			
338 RCL 08			
339 -			
340 /			

3

ROW 1 (1 : 2)



ROW 2 (3 : 5)



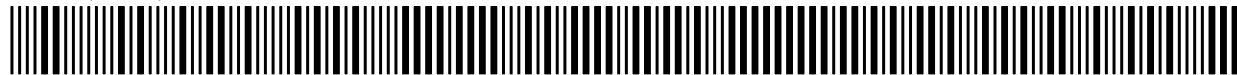
ROW 3 (5 : 12)



ROW 4 (12 : 16)



ROW 5 (16 : 20)



ROW 6 (20 : 25)



ROW 7 (25 : 27)



ROW 8 (27 : 33)



ROW 9 (33 : 37)



ROW 10 (37 : 40)



ROW 11 (41 : 45)



ROW 12 (46 : 47)



ROW 13 (48 : 56)



ROW 14 (56 : 59)



ROW 15 (60 : 65)



ROW 16 (66 : 74)



ROW 17 (75 : 80)



ROW 18 (80 : 85)



Psychrometric Properties

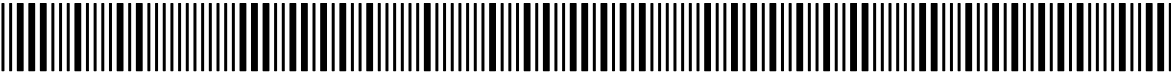
ROW 19 (86 : 91)



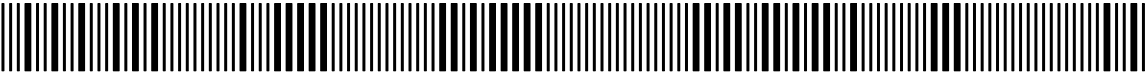
ROW 20 (91 : 97)



ROW 21 (98 : 106)



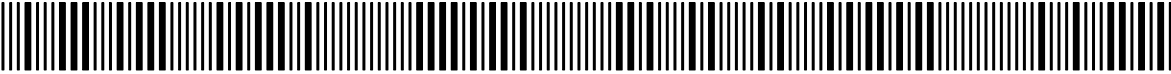
ROW 22 (107 : 112)



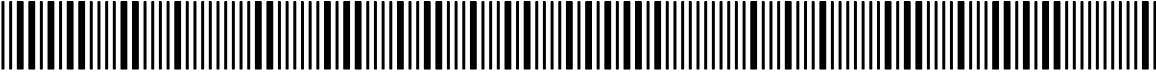
ROW 23 (113 : 120)



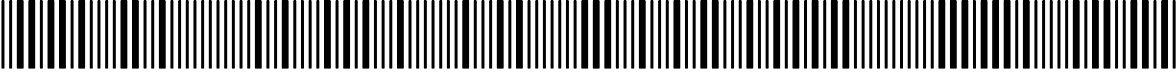
ROW 24 (121 : 126)



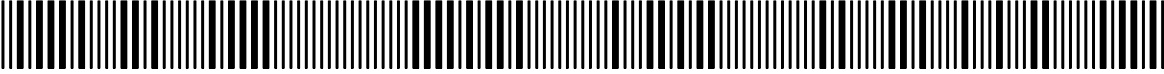
ROW 25 (126 : 130)



ROW 26 (131 : 138)



ROW 27 (139 : 143)



ROW 28 (143 : 151)



ROW 29 (151 : 153)



ROW 30 (153 : 161)



ROW 31 (162 : 170)



ROW 32 (170 : 177)



ROW 33 (177 : 184)



ROW 34 (184 : 186)



ROW 35 (186 : 191)



ROW 36 (191 : 193)

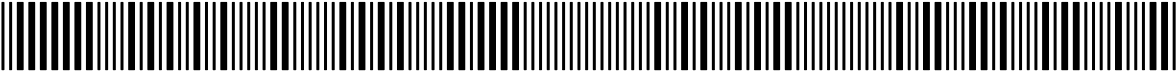


Psychrometric Properties

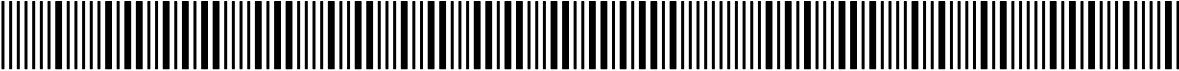
ROW 37 (194 : 198)



ROW 38 (198 : 204)



ROW 39 (204 : 206)



ROW 40 (206 : 211)



ROW 41 (211 : 215)



ROW 42 (216 : 220)



ROW 43 (220 : 228)



ROW 44 (228 : 231)



ROW 45 (232 : 236)



ROW 46 (236 : 241)



ROW 47 (241 : 243)



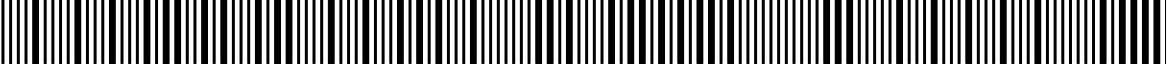
ROW 48 (243 : 249)



ROW 49 (249 : 254)



ROW 50 (254 : 256)



ROW 51 (256 : 261)



ROW 52 (261 : 263)



ROW 53 (264 : 267)



ROW 54 (267 : 274)

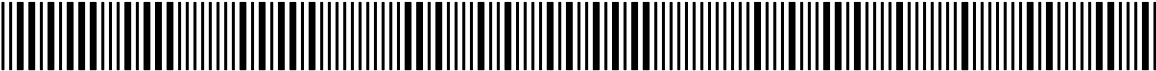


Psychrometric Properties

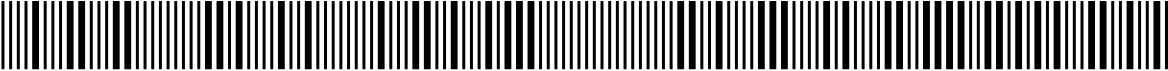
ROW 55 (275 : 285)



ROW 56 (286 : 289)



ROW 57 (290 : 298)



ROW 58 (298 : 304)



ROW 59 (305 : 309)



ROW 60 (310 : 314)



ROW 61 (314 : 321)



ROW 62 (322 : 328)



ROW 63 (328 : 332)



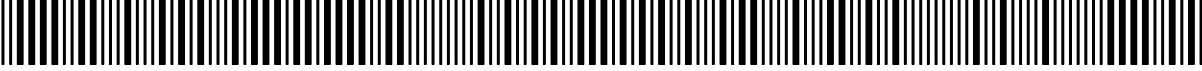
ROW 64 (332 : 335)



ROW 65 (336 : 344)



ROW 66 (344 : 349)



ROW 67 (349 : 355)



ROW 68 (356 : 363)



ROW 69 (363 : 368)



ROW 70 (369 - 369)



HEAT EXCHANGERS

(Requires one memory module)

This program allows analysis of counterflow, parallel flow, parallel-counterflow, and crossflow heat exchangers.

Figure 1:

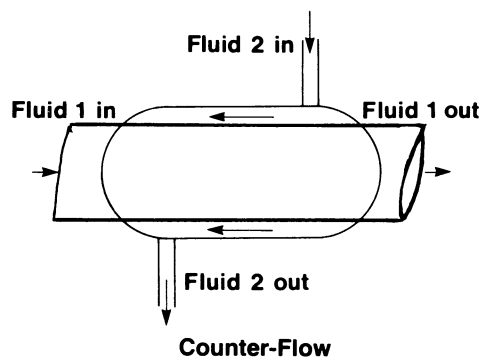


Figure 2:

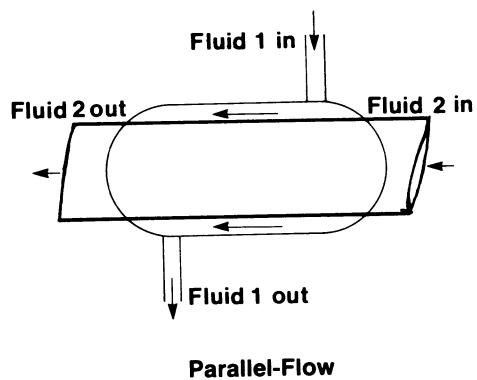


Figure 3:

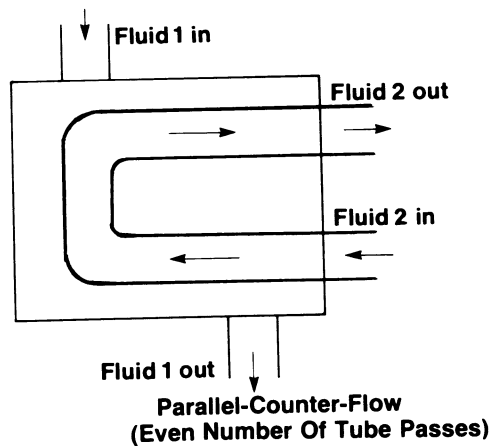
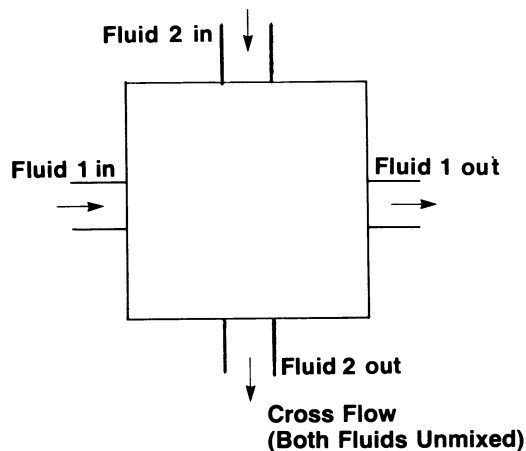


Figure 4:



Equations:

Heat exchanger effectiveness E is the ratio of actual heat transfer to maximum possible heat transfer.

$$E = \frac{Q}{C_{\min} (T_{hin} - T_{cin})} = \frac{C_h (T_{hin} - T_{ho})}{C_{\min} (T_{hin} - T_{cin})} = \frac{C_c (T_{co} - T_{cin})}{C_{\min} (T_{hin} - T_{cin})}$$

where:

Q is the actual heat transfer.

T_{hin} and T_{cin} are the inlet temperatures of the hot and cold fluids respectively.

T_{ho} and T_{co} are the outlet temperatures of the hot and cold fluids respectively.

C_h and C_c are the heat capacities of the hot and cold fluids, respectively, e.g., $C_h = \dot{m}_h \times c_{ph}$, where $\dot{m}_h$ is the flow rate and c_{ph} is the specific heat capacity of the hot fluid.

$C_{\min}$ and $C_{\max}$ (which are used later) are the smaller and larger values of C_h and C_c .

Effectiveness can be related to the product of the surface area of the heat exchanger and the overall heat transfer coefficient for specific geometries. This product is designated AU. The geometries considered in this pac have the following correlations:

Counterflow (see figure 1)

$$E = \frac{1 - e^{-\frac{AU}{C_{\min}} \left(1 - \frac{C_{\min}}{C_{\max}}\right)}}{1 - (C_{\min}/C_{\max})e^{-\frac{AU}{C_{\min}} \left(1 - \frac{C_{\min}}{C_{\max}}\right)}}$$

For $C_{\min}/C_{\max} = 1$

$$E = \frac{AU/C_{\min}}{1 + AU/C_{\min}}$$

Parallel Flow (see figure 2)

$$E = \frac{1 - e^{-\frac{AU}{C_{\min}} (1 + C_{\min}/C_{\max})}}{1 + C_{\min}/C_{\max}}$$

For $C_{\min}/C_{\max} = 0$, $C_{\min}$ is set to 1.

Parallel-Counterflow (well mixed with an even number of tube passes; see Figure 3)

$$E = \frac{2}{\left(1 + \frac{C_{\min}}{C_{\max}}\right) + \sqrt{1 + \left(\frac{C_{\min}}{C_{\max}}\right)^2} \left[\frac{1 + e^{-x}}{1 - e^{-x}}\right]}$$

where:

$$x = \frac{AU}{C_{\min}} \sqrt{1 + \left(\frac{C_{\min}}{C_{\max}}\right)^2}$$

Crossflow (both fluids unmixed; see figure 4)

No exact expression exists for this case, but the following is a very good approximation. Note that an iterative solution is required for AU.

$$E = 1 - e \left(e^{\left(-\frac{AU}{C_{\min}} \frac{C_{\min}}{C_{\max}} y \right)} - 1 \right) \left(\frac{C_{\max}}{C_{\min}} \frac{1}{y} \right)$$

where:

$$y = \left[\frac{C_{\min}}{AU} \right]^{0.22}$$

References:

W.M. Kays and A.L. London, *Compact Heat Exchangers*, National Press, 1955
 Eckert and Drake, *Heat and Mass Transfer*, McGraw-Hill.

Remarks:

For cases where the inlet and outlet temperatures of one of the fluids are equal(change of phase), use zero for the heat capacity of that fluid.

The solution for AU in the crossflow configuration takes significantly longer than other solutions because of the iterative technique required.

The program must be allowed to solve for all values (AU, Q, T_{co}, T_{ho}, and E). It is quite possible for the heat balance equations to yield physically meaningless solutions for a particular configuration. However, the message "2ND LAW ERR" will be displayed if the 2nd law of thermodynamics has been violated during the calculation of AU or Q.

This program is organized into five routines. The first routine performs heat balance calculations and acts as a controller for the four configuration subroutines. Each configuration subroutine has two sections that calculate AU and E for that heat exchanger. You should first load the controller, then load the configuration of interest as a separate program.

You may wish to write your own configuration routines. A routine for a configuration must be in the following format:

```

      LBL ACON
      •
      •
      •
      (calculates AU for this configuration)
      •
      •
      •
      RTN
      •
      •
      •
      LBL ECON
      •
      •
      •
      (calculates E for this configuration)
      •
      •
      •
      END

```

Example:

A liquid at 168°F is to be cooled to 117°F. The liquid has a heat capacity of 0.42 Btu/LBM-°F and flows at 7700 LBM/hr. Cooling water (heat capacity = 1.00) is available at 4800 lbm/hr at 50°F. For counterflow, crossflow, parallel-counterflow, and parallel flow heat exchangers with overall coefficients of 55 Btu/hr-ft²-°F what areas are required?

Keystrokes: (SIZE > 023)

Display:

[////] [FIX] 4

Load main routine and counterflow subroutine.

[XEQ] [ALPHA] HEATX [ALPHA]

TC IN=?

50 [R/S]

TH IN=?

168 [R/S]

MC=?

4800 [R/S]

MH=?

7700 [R/S]

CPC=?

1 [R/S]

CPH=?

.42 [R/S]

SELECT KEY: E AU Q TC TH

Since the temperature of the outgoing fluid is known, press the [E] key.

[E]

THO=?

117 [R/S]

E=0.4322

[R/S]*

AU=2,198.7662

[R/S]*

Q=164,933.9999

[R/S]*

TCO=84.3612

[R/S]*

SELECT KEY: E AU Q TC TH

Keystrokes:

Since $A = AU/U$, calculate A.

2198.7662 [ENTER] 55 [$\div$]

Load crossflow subroutine.

[XEQ] [ALPHA] HEATX [ALPHA]

[R/S]

[R/S]

[R/S]

[R/S]

[R/S]

[R/S]

[E]

[R/S]

[R/S]*

[R/S]*

[R/S]*

[R/S]

2353.6675 [ENTER] 55 [$\div$]

Display:

39.9776

TC IN=?

TH IN=?

MC=?

MH=?

CPC=?

CPH=?

SELECT KEY: E AU Q TC TH

THO=?

E=0.4322

AU=2,353.6675

Q=164,934.0000

TCO=84.3613

SELECT KEY: E AU Q TC TH

42.7940

An analogous procedure will yield areas of 42.2776 ft^2 and 45.1494 ft^2 for parallel-counterflow and parallel exchanges respectively.

User Instructions

				SIZE: 023
STEP	INSTRUCTIONS	INPUT	FUNCTION	DISPLAY
1.	Load program and then:		[GTO] ..	
2.	Load configuration subroutine corresponding			
	to your heat exchanger geometry		[XEQ] HEATX	TC IN=?
3.	Input inlet temperature of cold fluid	T_{cin}	[R/S]	TH IN=?
4.	Input inlet temperature of hot fluid	T_{hin}	[R/S]	MC=?
5.	Input mass flow rate of cold fluid	m_c	[R/S]	MH=?
6.	Input mass flow rate of hot fluid	m_h	[R/S]	CPC=?
7.	Input specific heat of cold fluid	C_{pc}	[R/S]	CPH=?
8.	Input specific heat of hot fluid	C_{ph}	[R/S]	SELECT KEY
				E AU Q TC TH
9.	Select the known value:			
	heat exchanger effectiveness		[A]	E=?
	area-heat transfer coefficient product		[B]	AU=?
	heat transfer		[C]	Q=?
	outlet temperature of cold fluid		[D]	TCO=?
	outlet temperature of hot fluid		[E]	THO=?
	input the known value.	E	[R/S]	
		AU	[R/S]	
		Q	[R/S]	
		TCO	[R/S]	
		THO	[R/S]	
	The four variables other than the one you			E=
	input will be output. The output order		[R/S]*	AU=
	will vary depending on which value was		[R/S]*	Q=
	input. If the 2nd law of thermodynamics		[R/S]*	TCO=
	is violated, the message "2ND LAW ERR"		[R/S]*	THO=
	will be displayed.		[R/S]*	SELECT KEY

[illegible]

Program Listings

Heat Exchanger - Main Routine

01♦LBL "HEA TX"	Input values.	49 XEQ "IN"	
02 2		50 ADV	
03 STO 00		51 GTO 16	
04 "TC IN"		52♦LBL B	
05 XEQ "IN"		53 SF 03	Input AU.
06 "TH IN"		54 10	
07 XEQ "IN"		55 STO 00	
08 14		56 "AU"	
09 STO 00		57 XEQ "IN"	
10 "MC"		58 ADV	
11 XEQ "IN"		59 GTO 01	
12 "MH"		60♦LBL C	
13 XEQ "IN"		61 SF 04	Input Q.
14 "CPC"		62 11	
15 XEQ "IN"		63 STO 00	
16 RCL 15		64 "Q"	
17 *		65 XEQ "IN"	
18 STO 05		66 ADV	
19 "CPH"		67 GTO 05	
20 XEQ "IN"		68♦LBL D	
21 RCL 16		69 SF 05	Input TCO.
22 *		70 12	
23 STO 06		71 STO 00	
24 "CON"		72 "TCO"	
25 ASTO 22	Select last input.	73 XEQ "IN"	
26♦LBL 06		74 ADV	
27 CF 02		75 GTO 14	
28 CF 03		76♦LBL E	
29 CF 04		77 SF 06	Input THO.
30 CF 05		78 13	
31 CF 06		79 STO 00	
32 CF 21		80 "THO"	
33 SF 27		81 XEQ "IN"	
34 "SELECT KEY:"		82 ADV	
35 AVIEW		83 GTO 04	
36 SF 21		84♦LBL 16	
37 PSE		85 FS?C 03	Calculate AU.
38♦LBL 00		86 GTO 06	
39 ADV		87 RCL 10	
40 "E AU Q TC TH"		88 "A"	
41 PROMPT		89 XEQ 08	
42 GTO 00		90 STO 11	
43♦LBL A		91 "AU"	
44 SF 02		92 XEQ "Q"	
45 9	Input E.	93♦LBL 01	Calculate Q.
46 STO 00		94 FS?C 04	
47 SF 01		95 GTO 06	
48 "E"		96 RCL 11	
		97 "E"	
		98 XEQ 08	
		99 RCL 07	

Program Listings

Heat Exchanger - Main Routine

100 *		151 X<>Y	
101 RCL 04		152 RCL 04	
102 RCL 03		153 RCL 03	
103 -		154 -	
104 *		155 /	
105 STO 12		156 RCL 05	
106 "Q"		157 RCL 06	
107 XEQ "O"		158 X<=Y?	
108♦LBL 05		159 X<>Y	
109 FS?C 05		160 RDN	
110 GTO 06	Calculate TCO.	161 X=0?	
111 RCL 12		162 X<> T	
112 RCL 05		163 /	
113 X≠0?		164 STO 10	
114 /		165 SF 01	
115 RCL 03		166 "E"	
116 +		167 XEQ "O"	
117 STO 13		168 GTO 16	
118 "TCO"		169♦LBL "A0"	
119 XEQ "O"		170 1	
120♦LBL 14		171 RCL 10	
121 FS?C 06		172 -	
122 GTO 06	Calculate THO.	173 LN	
123 RCL 13		174 CHS	A0 for $C_{\min}=0.00$.
124 RCL 03		175 RTN	
125 -		176♦LBL "E0"	
126 RCL 05		177 1	
127 *		178 RCL 11	
128 RCL 06		179 CHS	
129 X≠0?		180 E↑X	E0 for $C_{\min}=0.00$.
130 /		181 -	
131 RCL 04		182 RTN	
132 -		183♦LBL 08	
133 CHS		184 RCL 05	
134 STO 14		185 RCL 06	
135 "THO"		186 X>Y?	
136 XEQ "O"		187 X<>Y	
137♦LBL 04		188 X<>Y	
138 FS?C 02		189 STO 07	
139 GTO 06		190 X<>Y	
140 RCL 13	Calculate E.	191 X≠0?	
141 RCL 03		192 STO 07	
142 -		193 X<>Y	
143 RCL 05		194 X≠0?	
144 *		195 /	
145 RCL 04		196 STO 09	
146 RCL 14		197 SF 25	
147 -		198 X=0?	
148 RCL 06		199 "F0"	
149 *		200 X≠0?	
150 X=0?		201 ARCL 22	Find $C_{\min}$ and execute configuration subroutine.

Program Listings

202 ASTO T		51	
203 XEQ IND			
T			
204 FS?C 25			
205 RTN			
206 "2ND LAW			
ERR"	Trap errors from		
207 PROMPT	subroutines		
208 GTO 06			
209♦LBL "IN"			
210 CF 22	Input subroutine	60	
211 1			
212 ST+ 00			
213 RCL IND			
00			
214 "F="			
215 ASTO Y			
216 "F?"			
217 CF 21			
218 AVIEW			
219 SF 21		70	
220 CLA			
221 ARCL Y			
222 STOP			
223 STO IND			
00			
224 FS? 22			
225 FC? 55			
226 RTN			
227 ARCL X			
228 PRA		80	
229 RTN	Print if printer		
230♦LBL "O"	is attached		
231 "F="			
232 ARCL X	Output subroutine		
233 AVIEW			
234 .END.			
40		90	
50		00	

Program Listings

Parallel Flow Subroutine

01♦LBL "ACO N"	Calculate AU.	51	
02 RCL 09			
03 1			
04 +			
05 RCL 10			
06 *			
07 CHS			
08 1			
09 +		60	
10 LN			
11 CHS			
12 1			
13 RCL 09			
14 +			
15 /			
16 RCL 07			
17 *			
18 RTN			
19♦LBL "ECO N"	Calculate E.	70	
20 1			
21 +			
22 RCL 11			
23 RCL 07			
24 /			
25 *			
26 CHS			
27 E↑X			
28 CHS			
29 1		80	
30 +			
31 1			
32 RCL 09			
33 +			
34 /			
35 RTN			
40		90	
50		00	

Program Listings

Counter Flow Subroutine

01♦LBL "ACO N"	Calculate AU.	50 RCL 11 51 RCL 07 52 / 53 ENTER↑ 54 ENTER↑ 55 1 56 + 57 / 58 RTN	60	
02 RCL 10				
03 1/X				
04 -				
05 1				
06 LASTX				
07 -				
08 /				
09 LN				
10 1				
11 RCL 09				
12 -				
13 X=0?				
14 GTO 10				
15 /				
16 RCL 07				
17 *				
18 RTN				
19♦LBL 10	Calculate E.		70	
20 RCL 10				
21 1				
22 RCL 10				
23 -				
24 /				
25 RCL 07				
26 *				
27 RTN				
28♦LBL "ECO N"				
29 1			80	
30 -				
31 RCL 11				
32 RCL 07				
33 /				
34 *				
35 E↑X				
36 1				
37 X<>Y				
38 -				
39 LASTX			90	
40 RCL 09				
41 *				
42 1				
43 X<>Y				
44 -				
45 X=0?				
46 GTO 11				
47 /				
48 RTN				
49♦LBL 11			00	

Program Listings

Parallel-Counter Flow Subroutine

01♦LBL "ACO
N"

02 XEQ 12
03 2
04 *
05 RCL 12
06 2
07 RCL 10
08 /
09 +
10 RCL 08
11 -
12 /
13 CHS
14 1
15 +
16 LN
17 RCL 12
18 /
19 CHS
20 RCL 07
21 /
22 LASTX
23 X↑2
24 *
25 RTN
26♦LBL "ECO

N"

27 XEQ 12
28 RCL 11
29 RCL 07
30 /
31 RCL 12
32 *
33 CHS
34 E↑X
35 1
36 X<>Y
37 +
38 1
39 LASTX
40 -
41 /
42 RCL 12
43 *
44 RCL 08
45 +
46 2
47 X<>Y
48 /
49 RTN

Calculate AU.

50♦LBL 12
51 RCL 09
52 1
53 +
54 STO 08
55 RCL 09
56 X↑2
57 1
58 +
59 SQRT
60 STO 12
61 RTN

70

80

90

00

Calculate E.

Program Listings

Cross Flow Subroutine

01♦LBL "ACO N"	Calculate AU.	49 E↑X	
02 0		50 1	
03 STO 19		51 -	
04 1		52 *	
05 RCL 10		53 E↑X	
06 CHS		54 CHS	
07 STO 21		55 1	
08 +		56 +	
09 LN			
10 CHS		60	
11 STO 11			
12♦LBL 13			
13 RCL 11			
14 XEQ "ECO N"			
15 RCL 10			
16 -			
17 STO 20			
18 RCL 19			
19 RCL 11		70	
20 STO 19			
21 -			
22 RCL 21			
23 RCL 20			
24 STO 21			
25 -			
26 /			
27 *			
28 ST- 11			
29 ABS		80	
30 1 E-4			
31 X<=Y?			
32 GTO 13			
33 RCL 11			
34 RTN			
35♦LBL "ECO N"			
36 RCL 11	Calculate E.		
37 RCL 07			
38 /		90	
39 ENTER↑			
40 ENTER↑			
41 .22			
42 Y↑X			
43 RCL 09			
44 /			
45 /			
46 LASTX			
47 X<>Y			
48 CHS		00	

DATA REGISTERS				STATUS			
00	Storage Index	50		SIZE	23	TOT. REG.	102
				ENG		FIX	
				DEG		RAD	
	TC IN						
	TH IN						
05	CC	55		FLAGS			
	CH			#	INIT S/C	SET INDICATES	CLEAR INDICATES
	Cmin			0		Unit conversion	
	Cmax			1	C		
	Cmin/Cmax			2	C		
10	E	60		3	C		
	AU			4	C		
	Q			5	C		
	Tco			6	C		
	Tho			23		Alpha input	
15	MC	65		55		Printer connected	
	MH						
	cpc						
	cph						
	(AU _{i-1})						
20	F(AU _i)	70					
	F(AU _{i-1})						
	"CON"						
25		75					
30		80					
35		85					
				ASSIGNMENTS			
				FUNCTION	KEY	FUNCTION	KEY
40		90					
45		95					

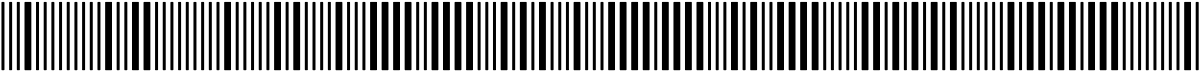
ROW 1 (1 : 4)	
ROW 2 (4 : 6)	
ROW 3 (6 : 11)	
ROW 4 (11 : 14)	
ROW 5 (15 : 20)	
ROW 6 (20 : 26)	
ROW 7 (27 : 33)	
ROW 8 (33 : 34)	
ROW 9 (35 : 40)	
ROW 10 (40 : 44)	
ROW 11 (45 : 51)	
ROW 12 (51 : 57)	
ROW 13 (57 : 64)	
ROW 14 (64 : 70)	
ROW 15 (70 : 75)	
ROW 16 (76 : 81)	
ROW 17 (81 : 88)	
ROW 18 (88 : 94)	

Heat Exchangers (Main Program)

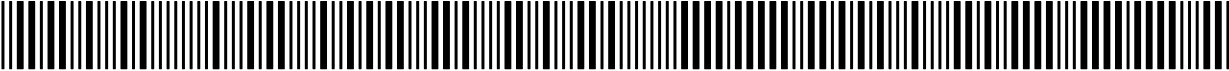
ROW 19 (94 : 102)



ROW 20 (103 : 110)



ROW 21 (111 : 119)



ROW 22 (119 : 129)



ROW 23 (130 : 137)



ROW 24 (138 : 148)



ROW 25 (149 : 161)



ROW 26 (162 : 168)



ROW 27 (168 : 175)



ROW 28 (176 : 183)



ROW 29 (184 : 196)



ROW 30 (197 : 203)



ROW 31 (204 : 206)



ROW 32 (206 : 210)



ROW 33 (211 : 216)



ROW 34 (217 : 224)



ROW 35 (225 : 230)



ROW 36 (231 - 234)



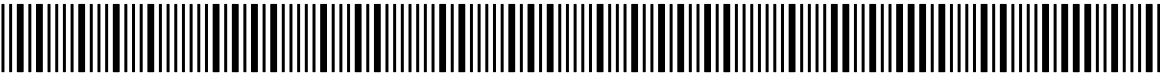
Heat Exchangers Parallel Flow Subroutine

Registers: 8

ROW 1 (1 : 6)



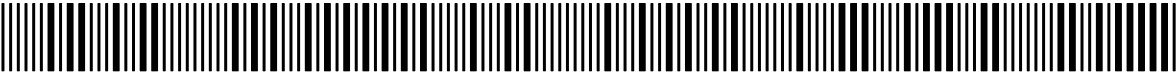
ROW 2 (7 : 19)



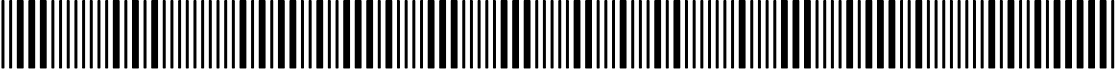
ROW 3 (19 : 25)



ROW 4 (26 : 36)



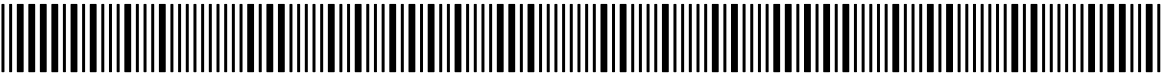
Heat Exchangers Counter Flow Subroutine Registers: 11

ROW 1 (1 : 6)	
ROW 2 (7 : 18)	
ROW 3 (19 : 28)	
ROW 4 (28 : 37)	
ROW 5 (38 : 49)	
ROW 6 (50 - 59)	

ROW 1 (1 : 4)



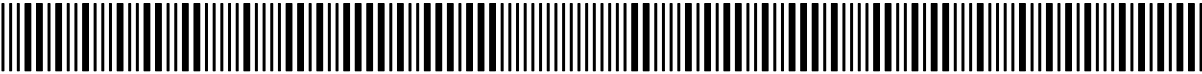
ROW 2 (5 : 17)



ROW 3 (18 : 26)



ROW 4 (26 : 34)



ROW 5 (35 : 47)



ROW 6 (48 : 60)



ROW 7 (61 - 62)



Heat Exchangers Cross Flow Subroutine

Registers: 14

ROW 1 (1 : 5)



ROW 2 (6 : 14)



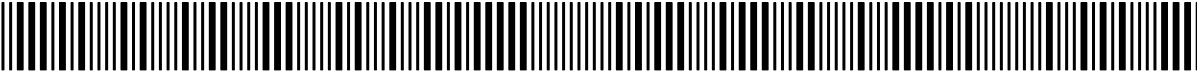
ROW 3 (14 : 22)



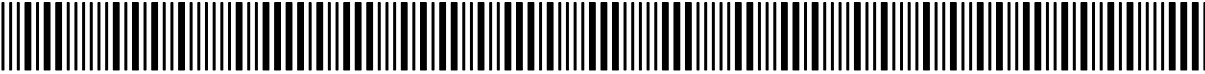
ROW 4 (22 : 30)



ROW 5 (30 : 35)



ROW 6 (35 : 44)



ROW 7 (45 : 57)



ROW 8 (57 - 57)



DECIBEL ADDITION AND SUBTRACTION

This program adds or subtracts sound pressure levels measured in decibels.

Equations:

$$dB_1 + dB_2 = 10 \log (10^{dB_1/10} + 10^{dB_2/10})$$

$$dB_1 - dB_2 = 10 \log (10^{dB_1/10} - 10^{dB_2/10})$$

When subtracting, if $dB_1 < dB_2$, the program will exchange values.

Example 1:

A noise level of 72 decibels is measured in a room. The air conditioning is turned on and the noise level increases to 74 decibels. What is the noise level of the air conditioning system.

Keystrokes:

Display:

[///] [FIX] 2

74 [ENTER] 72 [XEQ] [ALPHA] dB- [ALPHA] 69.67 dB

Example 2:

A compressor is known to have a sound pressure level of 90 dB. The background is 85 dB. What is the total?

Keystrokes:

Display:

[///] [FIX] 2

90 [ENTER] 85 [XEQ] [ALPHA] dB+ [ALPHA] 91.19dB

[illegible]

Program Listings

01♦LBL "dB+	Add decibels.	51	
02 XEQ 00			
03 +			
04 GTO 01	Subtract decibels.		
05♦LBL "dB-			
06 XEQ 00			
07 -	Display result.	60	
08 ABS			
09♦LBL 01			
10 LOG			
11 10			
12 *			
13 CLA			
14 ARCL X			
15 "F dB"			
16 AVIEW			
17 RTN	Convert for add or subtract.	70	
18♦LBL 00			
19 10			
20 ST/ Z			
21 /			
22 X<>Y			
23 10↑X			
24 X<>Y			
25 10↑X			
30		80	
40		90	
50		00	

DATA REGISTERS				STATUS			
00		50		SIZE <u>ANY</u>	TOT. REG. <u>07</u>	USER MODE	
				ENG _____	FIX _____	SCI _____	ON _____ OFF _____
				DEG _____	RAD _____	GRAD _____	
05		55		FLAGS			
				#	INIT S/C	SET INDICATES	CLEAR INDICATES
10		60					
15		65					
20		70					
25		75					
30		80					
35		85					
40		90		ASSIGNMENTS			
				FUNCTION	KEY	FUNCTION	KEY
				(suggested)			
				dB+	-61		
				dB-	-51		
45		95					

ROW 1 (1 : 4)



ROW 2 (5 : 9)



ROW 3 (10 : 16)



ROW 4 (17 : 26)



ROW 5 (26 - 26)



TEMPERATURE CONVERSION

This program converts interchangeably between the four types of temperature.

Equations:

$$K = (^{\circ}F + 459.67)/1.8$$

$$K = ^{\circ}C + 273.15$$

$$K = ^{\circ}R / 1.8$$

where:

K is temperature in Kelvins.

$^{\circ}F$ is temperature in degrees Fahrenheit.

$^{\circ}C$ is temperature in degrees Celsius.

$^{\circ}R$ is temperature in degrees Rankine.

Remarks:

Only the stack registers, LASTx and the alpha register are used in the conversions.

Example:

Convert: 472K to $^{\circ}R$
 27 $^{\circ}F$ to $^{\circ}C$
 25 $^{\circ}C$ to $^{\circ}F$
 100 $^{\circ}C$ to $^{\circ}F$

Keystrokes:

[////] [FIX] 2
 [XEQ] [ALPHA] TCON [ALPHA]
 472 [D]
 [C]
 [R/S]
 27 [A]
 [B]
 25 [B]
 [A]
 100 [B]
 [A]

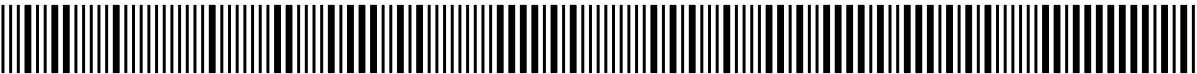
Display:

F	C	R	K	
F	C	R	K	
849.60				($^{\circ}R$)
F	C	R	K	
F	C	R	K	
-2.78				($^{\circ}C$)
F	C	R	K	
77				($^{\circ}F$)
F	C	R	K	
212				($^{\circ}F$)

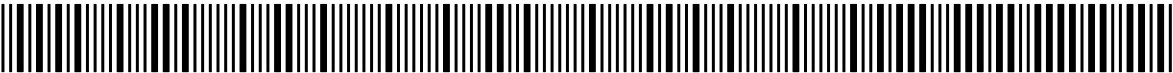
REGISTERS, STATUS, FLAGS, ASSIGNMENTS

[illegible]

ROW 1 (1 : 5)



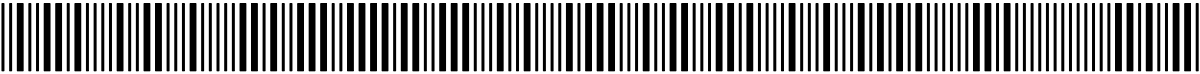
ROW 2 (5 : 7)



ROW 3 (8 : 12)



ROW 4 (12 : 16)



ROW 5 (17 : 23)



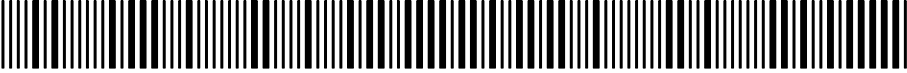
ROW 6 (23 : 28)



ROW 7 (29 : 33)



ROW 8 (33 - 37)



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HEAT EXCHANGERS
DECIBEL ADDITION AND SUBTRACTION
TEMPERATURE CONVERSIONS



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